

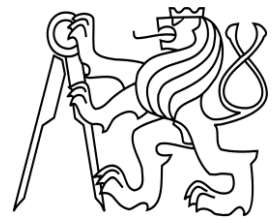
ADVANCED DESIGN FIRE MODELS

Travelling fire

Ing. Kamila Cábová, Ph.D.



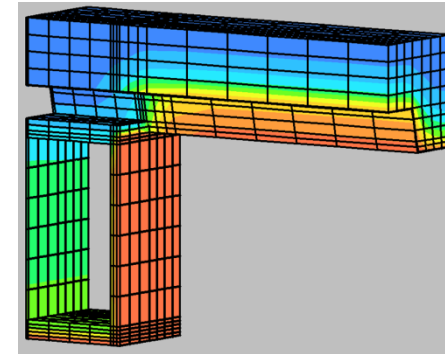
Fire design of structures



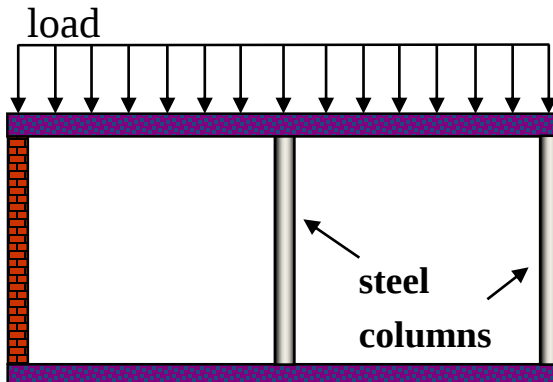
1: Ignition



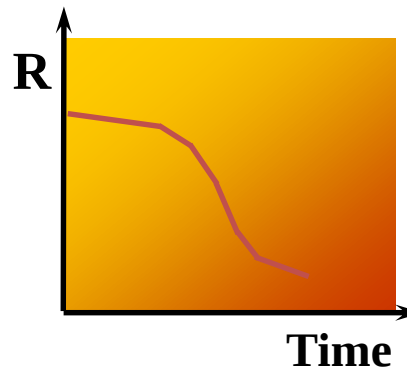
2: Thermal analysis



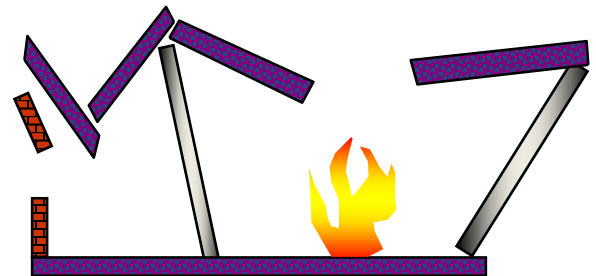
3: Temperature of the structure



4: Mechanical load

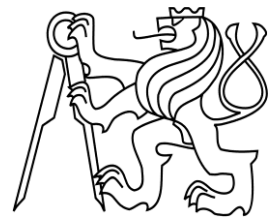


5: Structural analysis

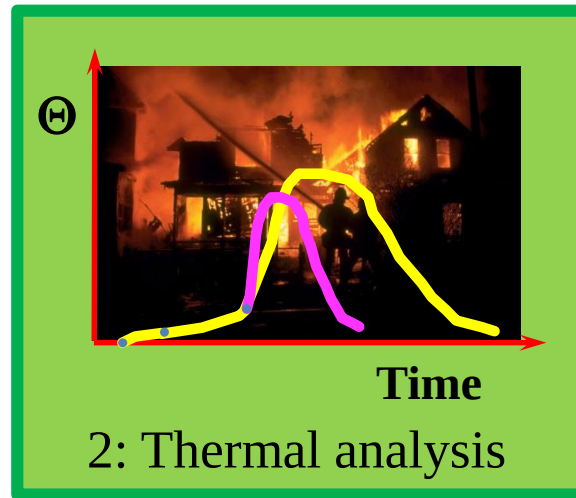


6: Collapse?

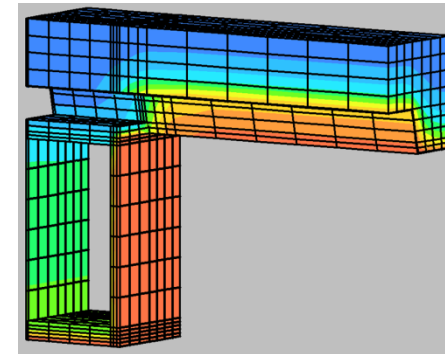
Thermal analysis



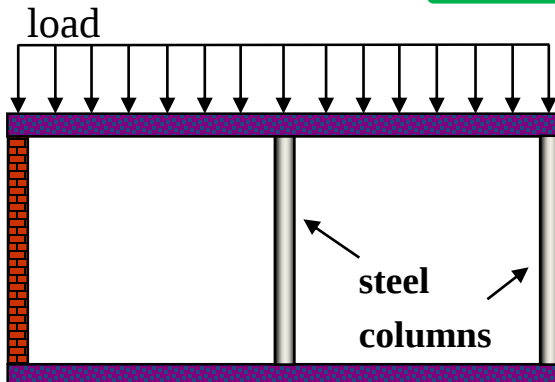
1: Ignition



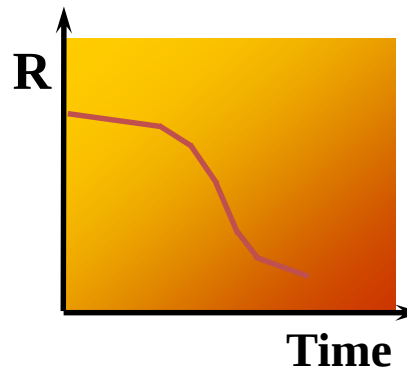
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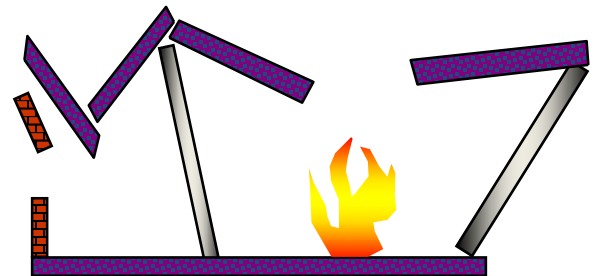
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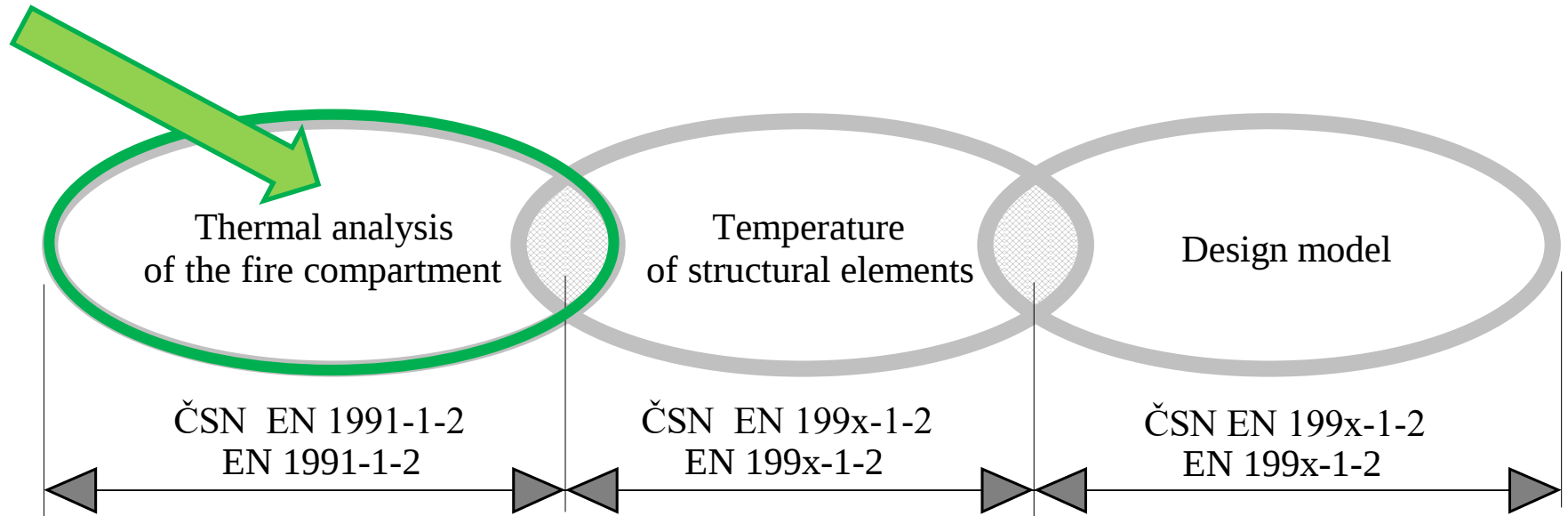
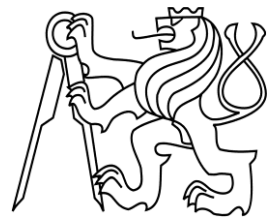


5: Structural analysis



6: Collapse?

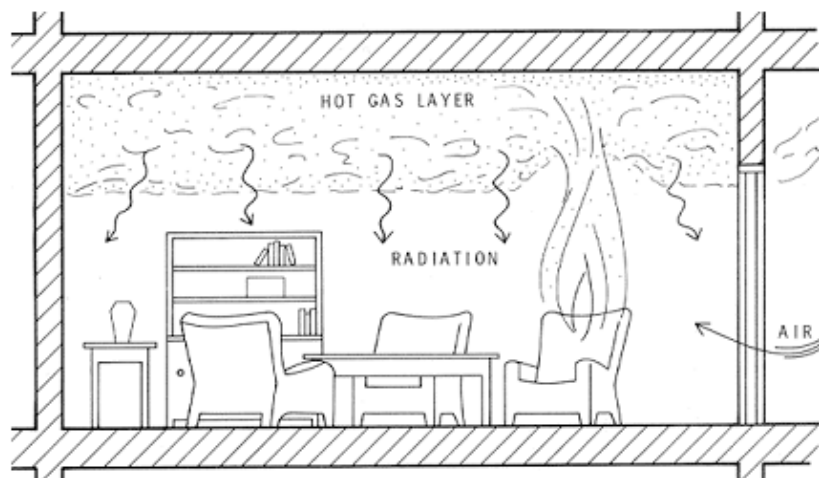
Thermal analysis



The principles and methods for thermal analysis are given in EN 1991-1-2.



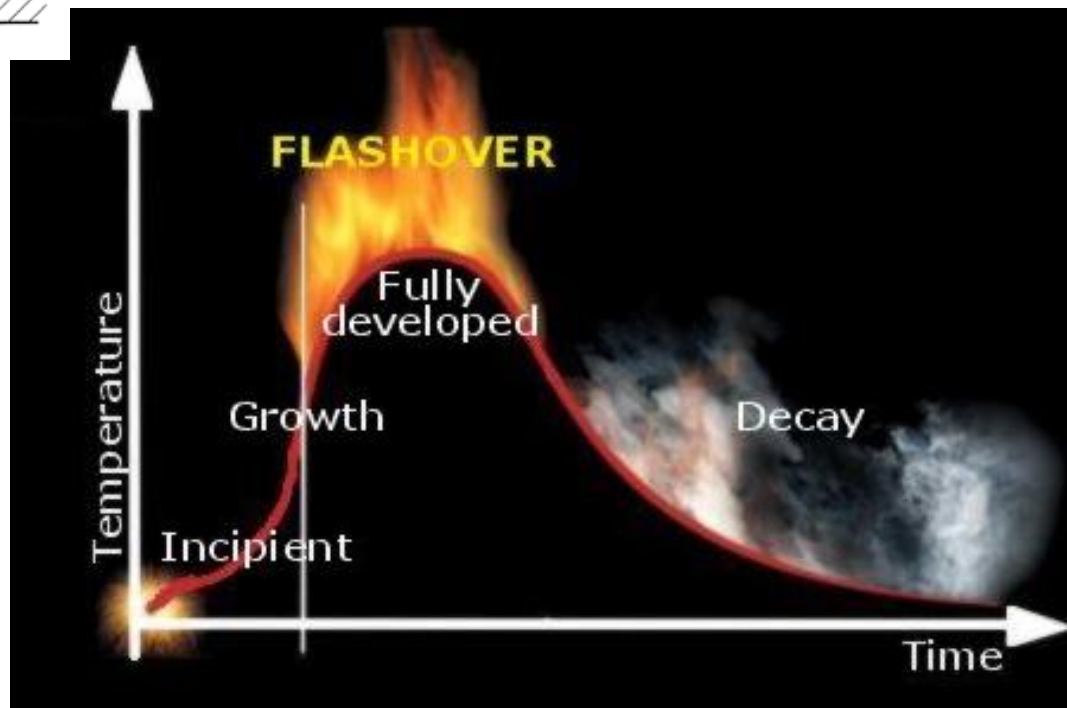
Compartment fire



Flashover – as the hot gas layer increases all combustibles are heated by radiation. If the temperature is enough high, the room breaks out into open flame at once. It generates big heat, smoke and pressure (window breakage).

Phases of the fire

- ignition
- smouldering
- flash over
- heating
- cooling

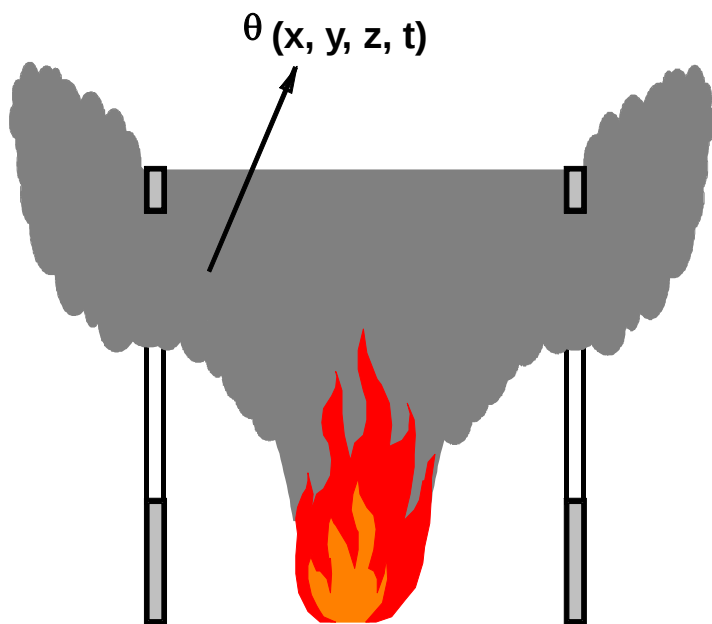




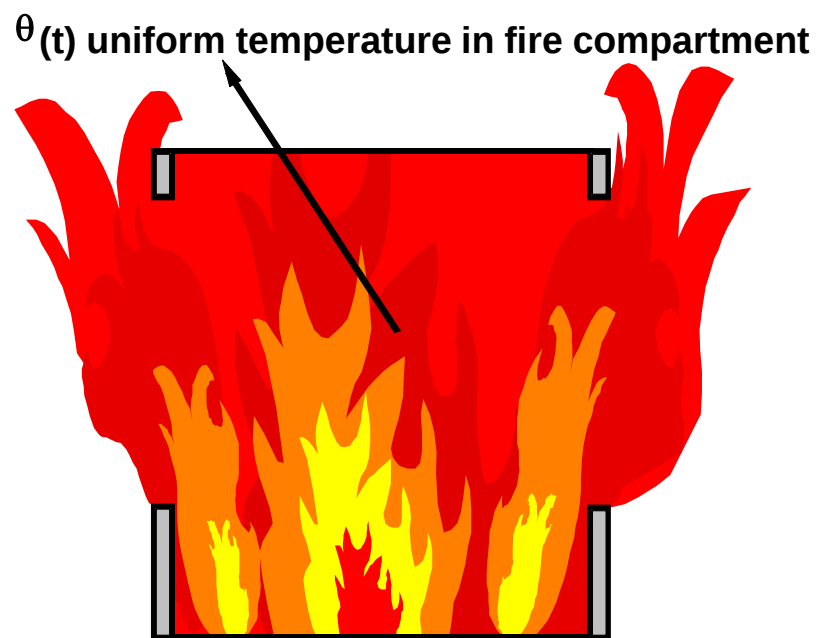
Modelling of fire

What kind of the fire? Is there flashover or not?

Localised fire



Compartment fire





Design fire models

According to EN 1991-1-2

Simple models

- ⇒ nominal curves
 - standard temperature-time curve (ISO 834)
 - hydrocarbon temperature-time curve
 - external temperature-time curve
- ⇒ parametric curve

Advanced models

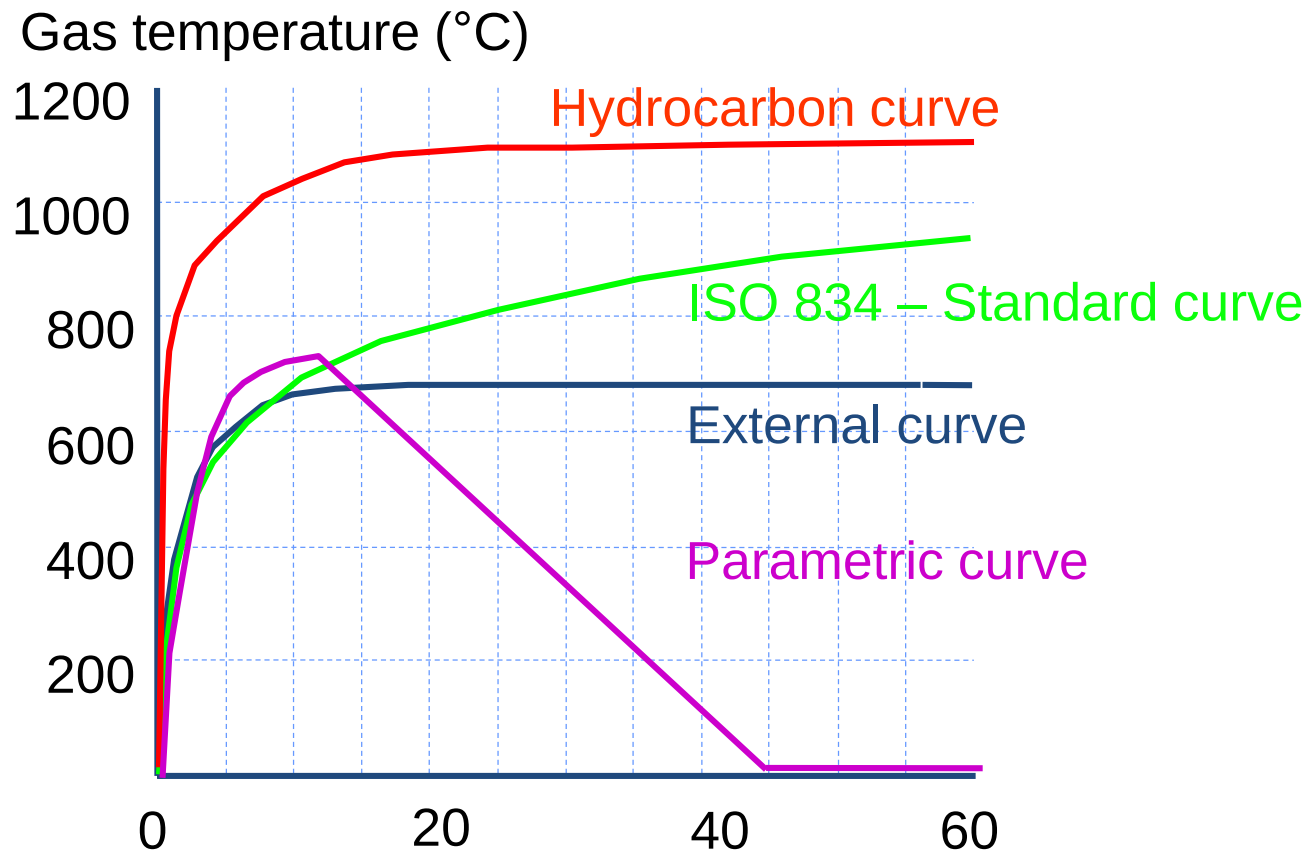
- ⇒ localised fire
- ⇒ one zone model
- ⇒ two zone model
- ⇒ CFD model



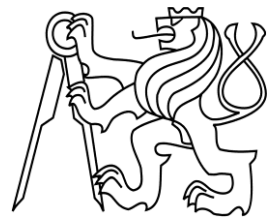


Simple design fire models

- Simple models

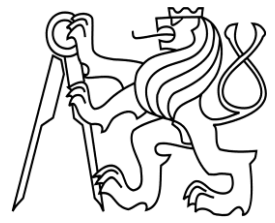


Advanced design fire models

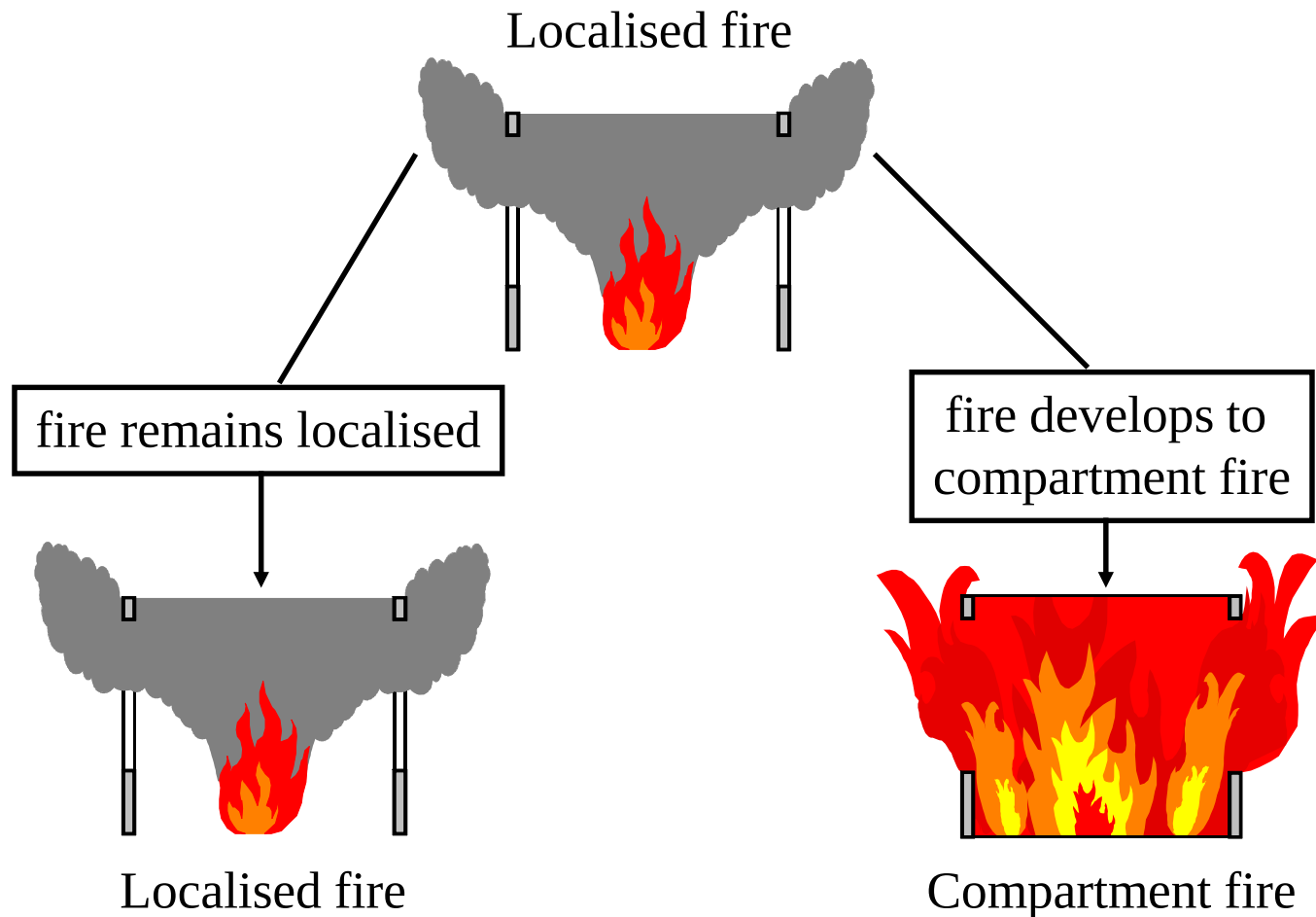


- **Advanced models**
 - Local fires
 - One zone model
 - Two zone model
 - CFD models

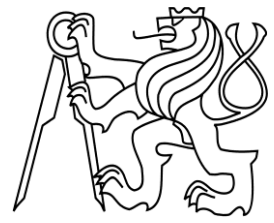
Advanced design fire models



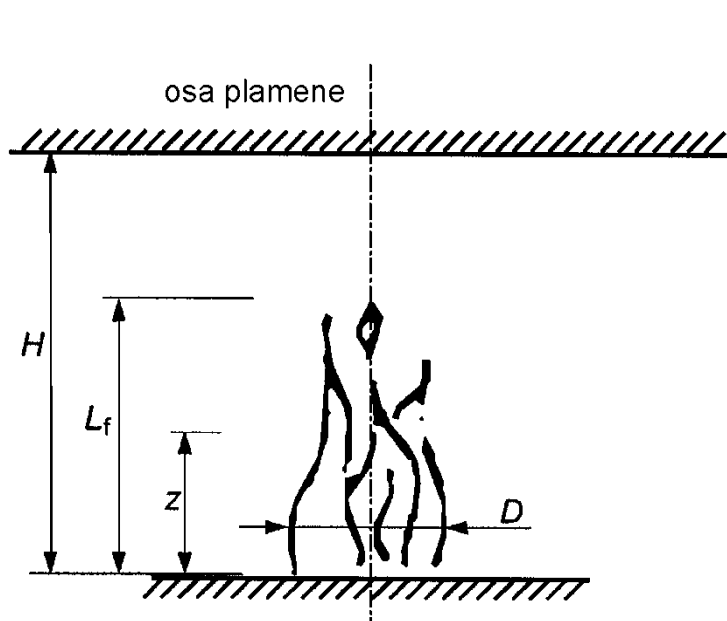
- Local fire and zone models



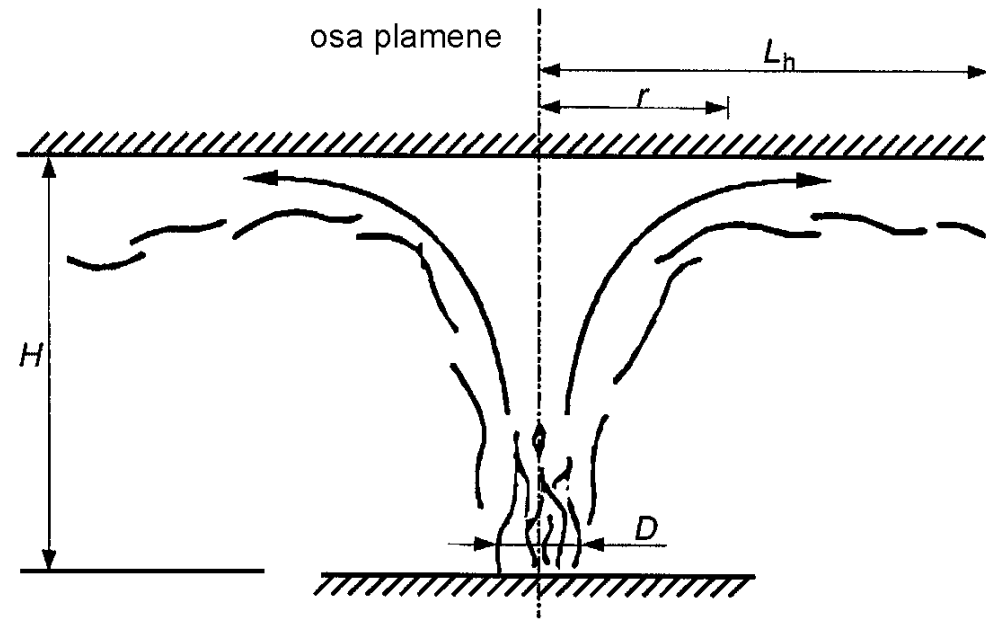
Advanced design fire models



- Local fire models



the flame does not reach the ceiling
(Heskestad)

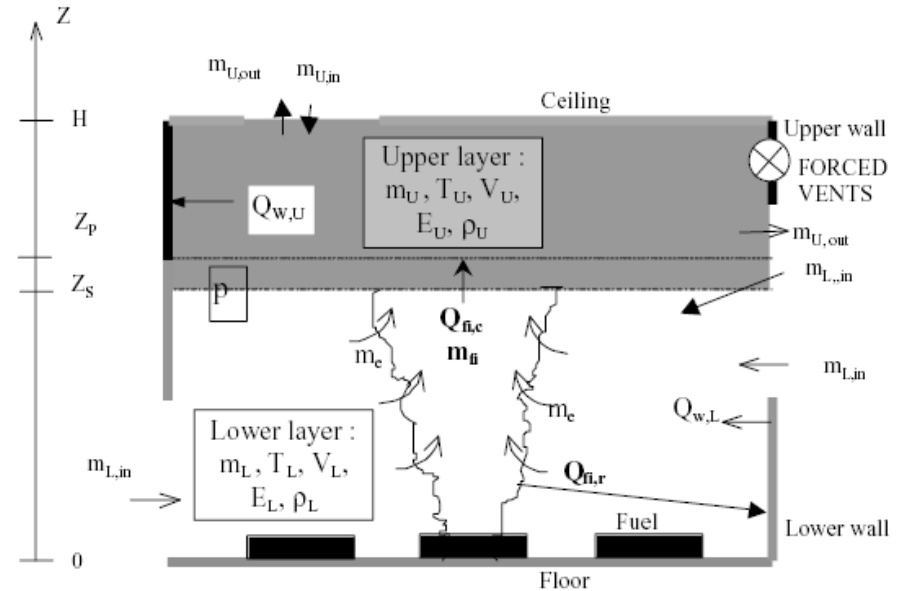
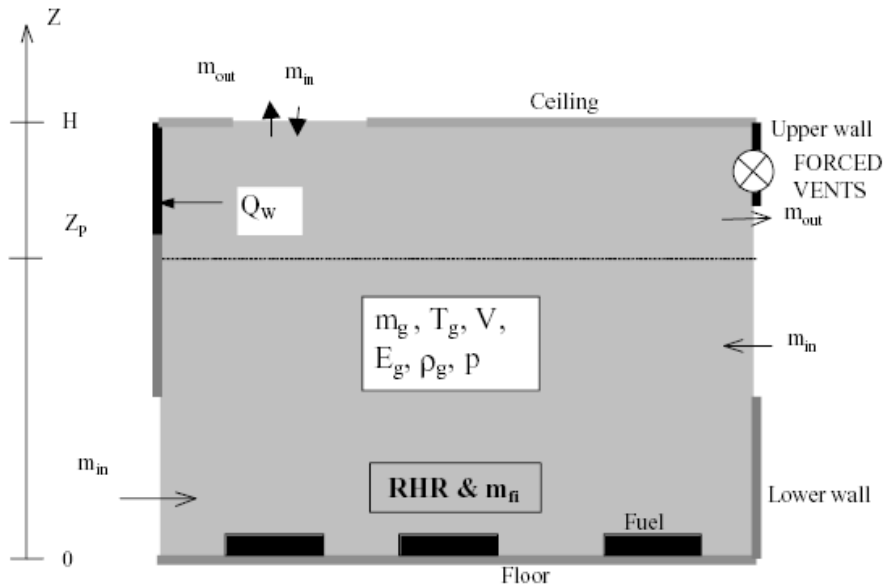


the flame impacts the ceiling
(Hasemi)

Advanced design fire models



- Zone models



Software available:

- OZONE, C-FAST, Argos, ...

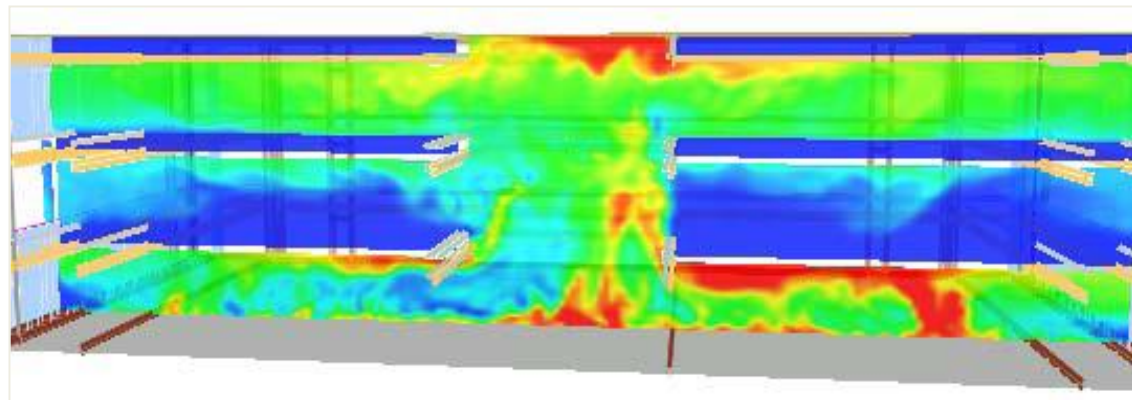
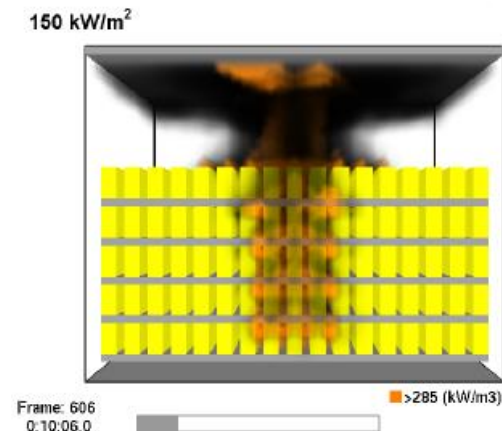
Advanced design fire models



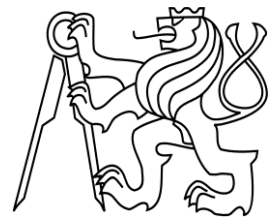
- Computational Fluid Dynamics models (CFD)

Principles:

- numerical solution of partial differential equations
thermodynamic and aerodynamic variables
at any location in the compartment
- mathematical description of equations:
 - mass balance of gas and fuel;
 - energy balance;
 - Newton's law
 -

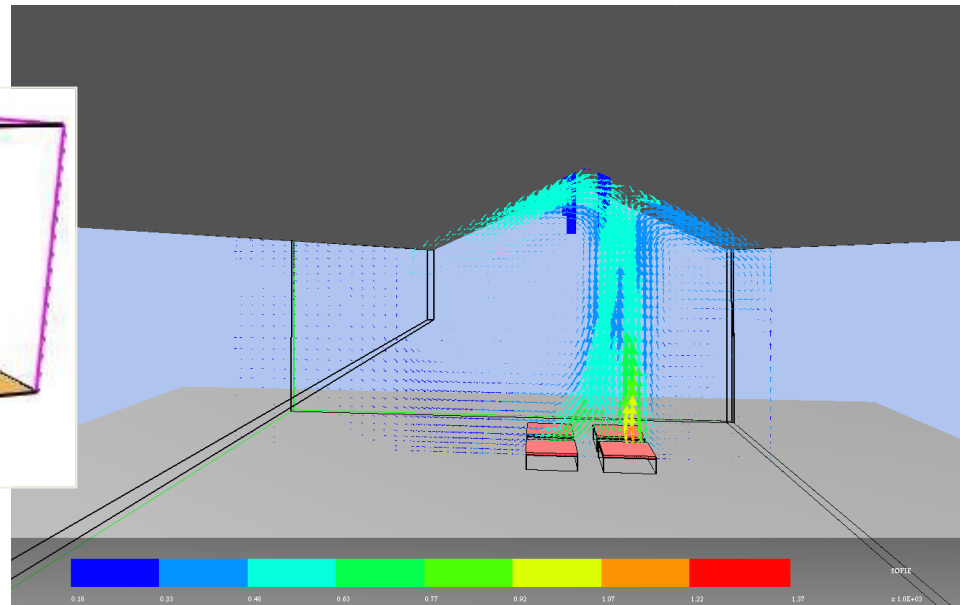
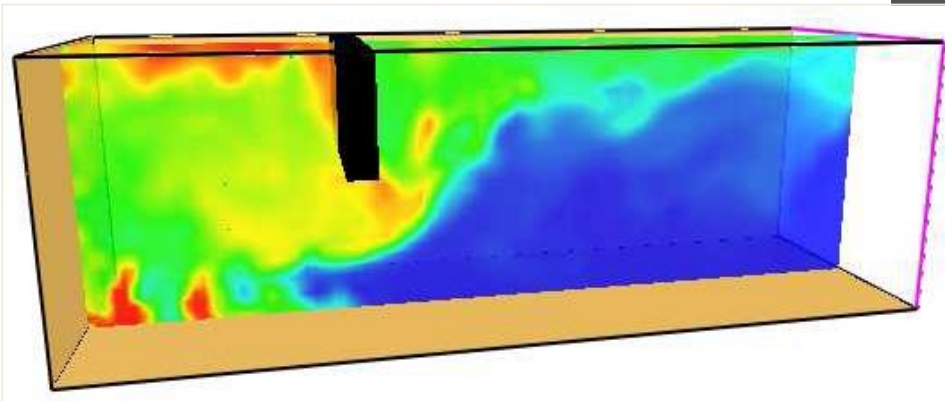


Advanced design fire models

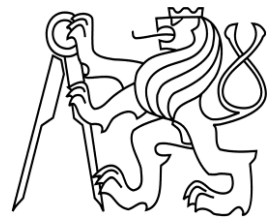


CFD models

- + Complicated geometry, all materials, prediction of smoke development, verification/validation needed
- Hardware demands, huge amount of input/output data, long computational time



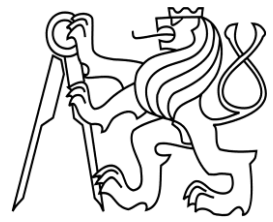
Application of design fire models



Application

- **Nominal curves**
for heating phase in simple cases
- **Parametric temperature curve**
also for cooling phase
- **Zone models**
for difficult geometry, ventilation conditions

Application of design fire models



Application

- **Local fire models**

new application also to vertical members (columns)

- **CFD models**

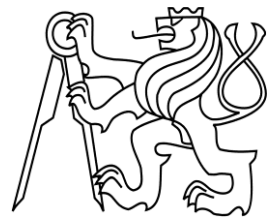
for all types of fires

difficult geometry, boundary conditions

for large space buildings

cost and time consuming

Design fire models

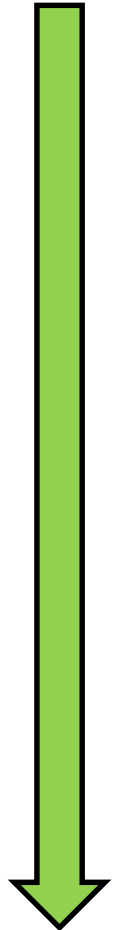


Simple models

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 - hydrocarbon temperature-time curve
 - external temperature-time curve
- ➡ parametric curve

Advanced models

- ➡ localised fire
- ➡ one zone model
- ➡ two zone model
 - models of travelling fire
- ➡ CFD model

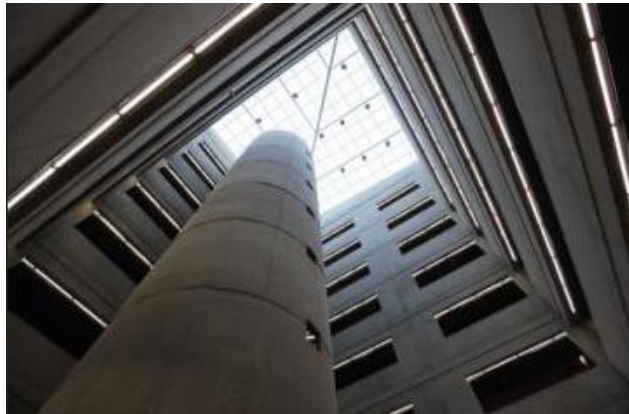


Travelling fire - motivation



Increase of architectural demands

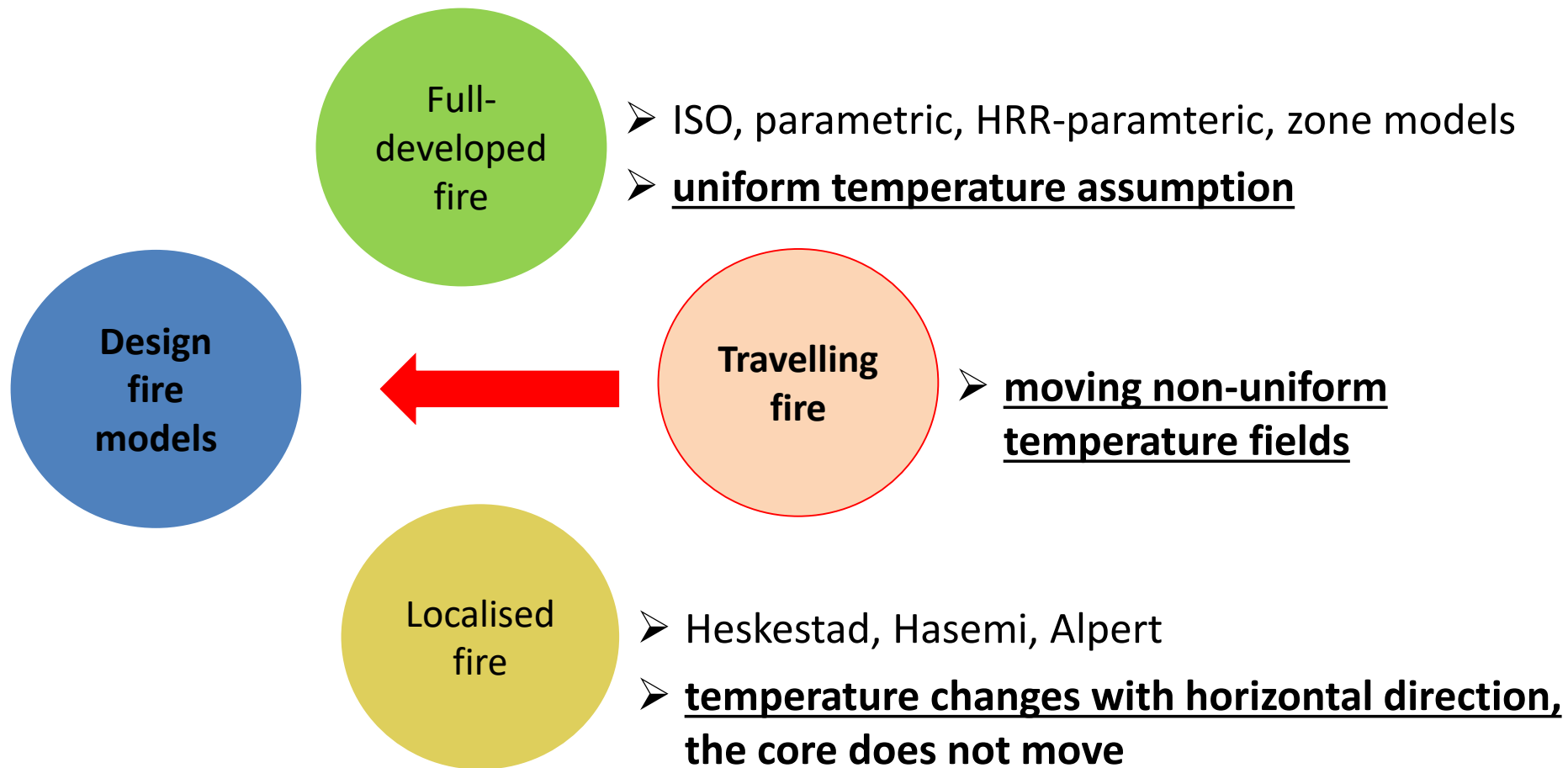
- Missing compartmentalization
 - Large open spaces
 - Connected floors, atria
- Modern materials





Travelling fire - motivation

Extension of design fire models





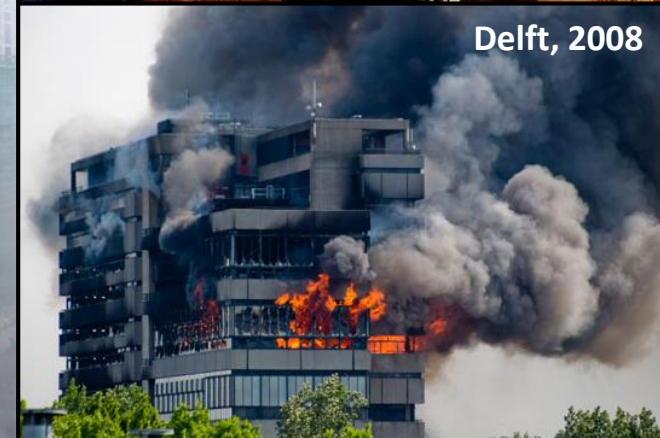
Travelling fire - motivation

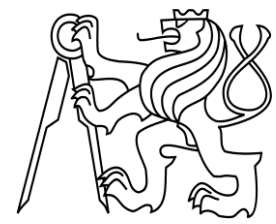
Travelling fire

- In real fires and experiments
- Fields with higher and lower temperatures, longer duration
- Closer to real fire behaviour



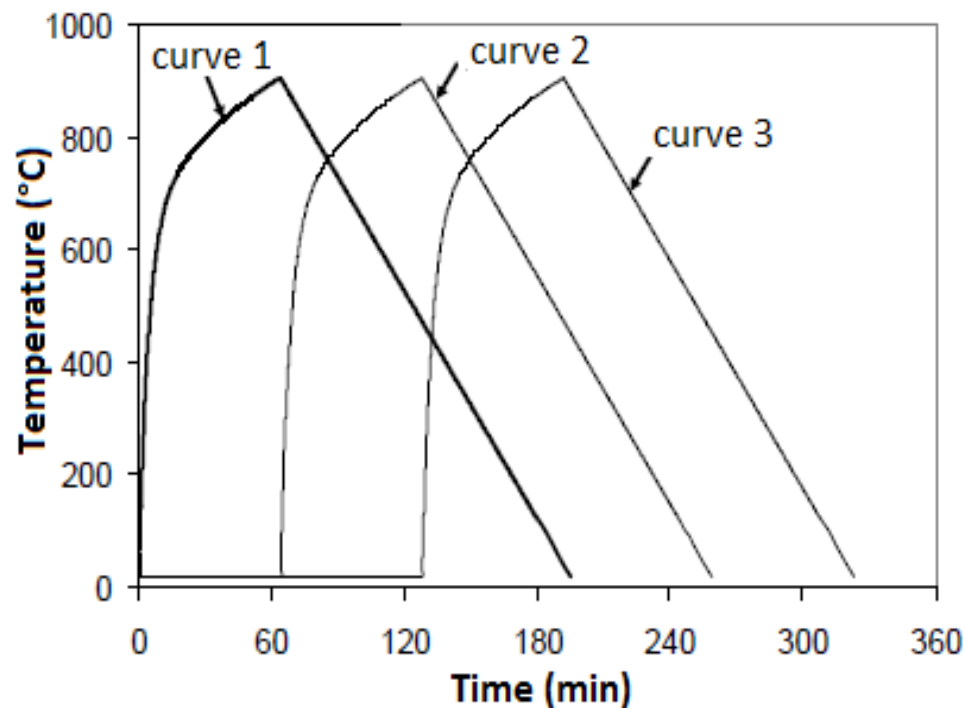
Design fire models of TF





Models of travelling fire

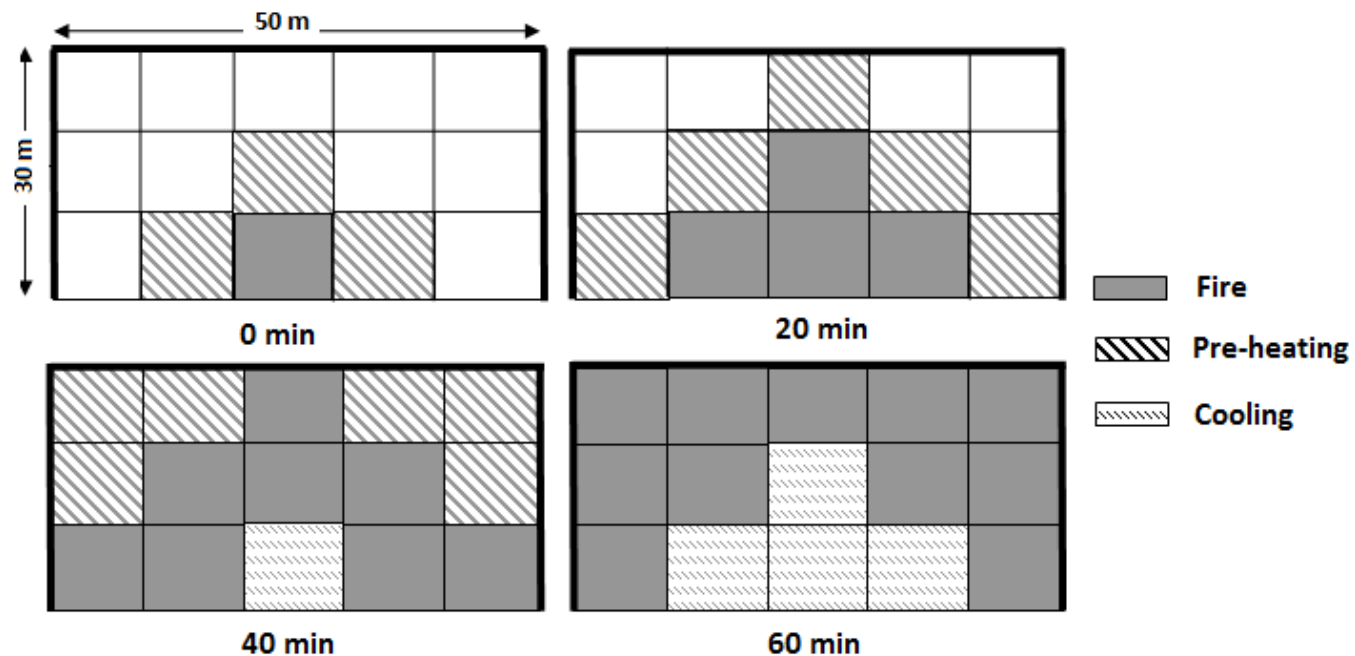
- Bailey (1996)
 - Parametric temperature-time curve
 - Time offset equal to peak temperature





Models of travelling fire

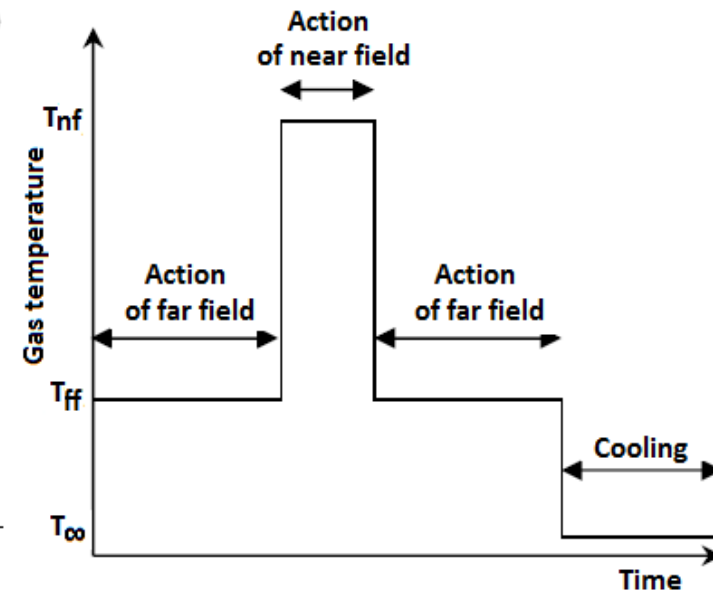
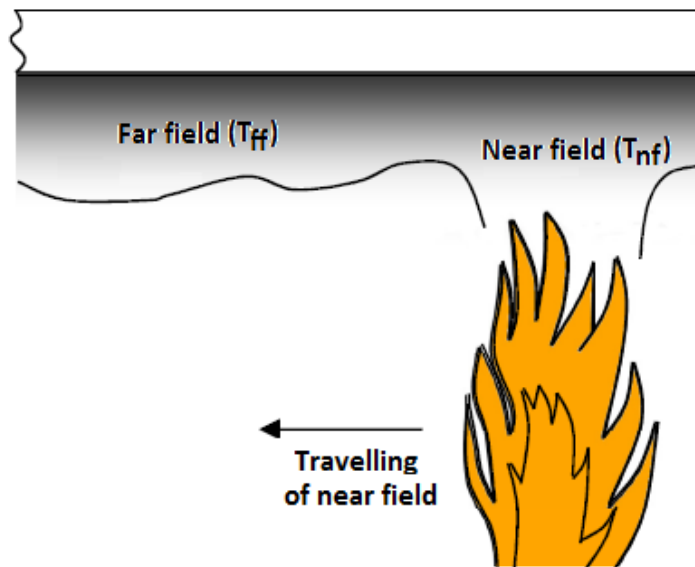
- Clifton (1996)
 - Design areas with fully-developed burning
 - Parametric temperature-time curve
 - Moving into next area in 20 min

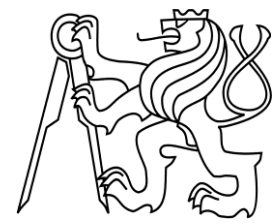




Models of travelling fire

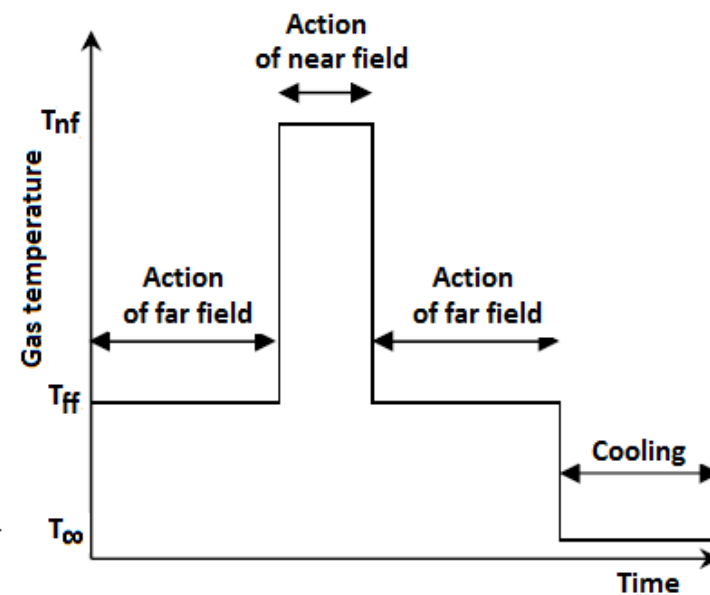
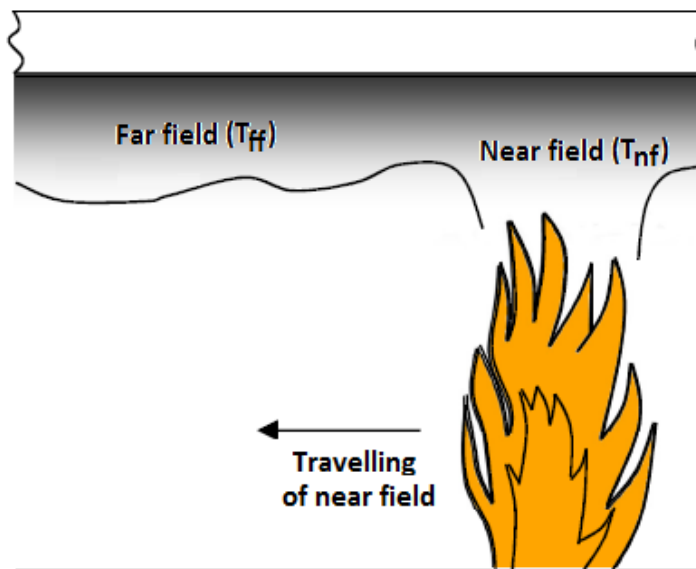
- Rein, Stern-Gottfried (2007) - TFM
 - Near-field temperature (flames, 1200 °C)
 - Far-field temperature (hot layer gases)
 - Description of various sizes of fire (from 1 % to 100 %)
 - Fire spread along longer side of an enclosure





Models of travelling fire

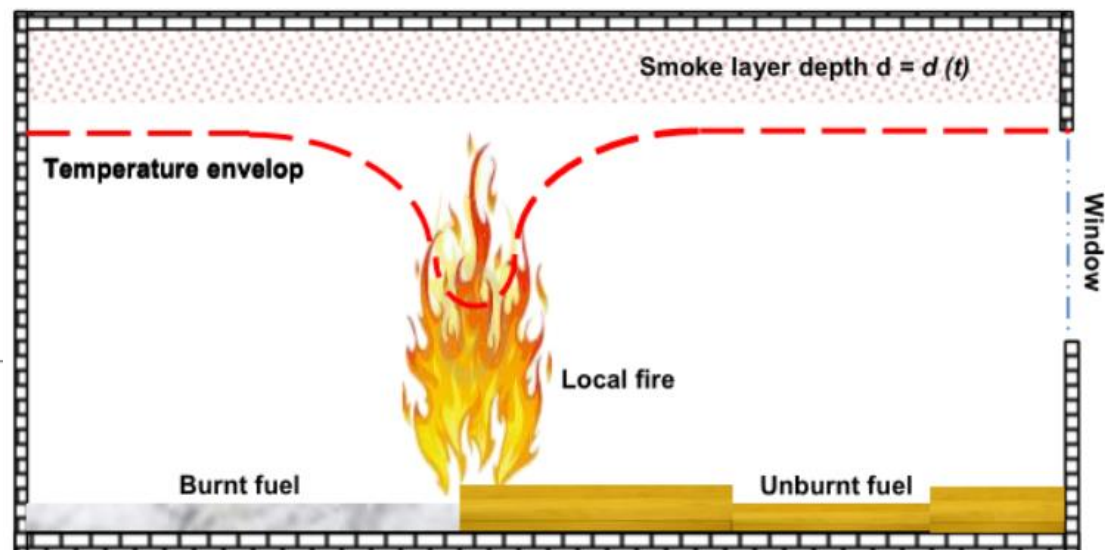
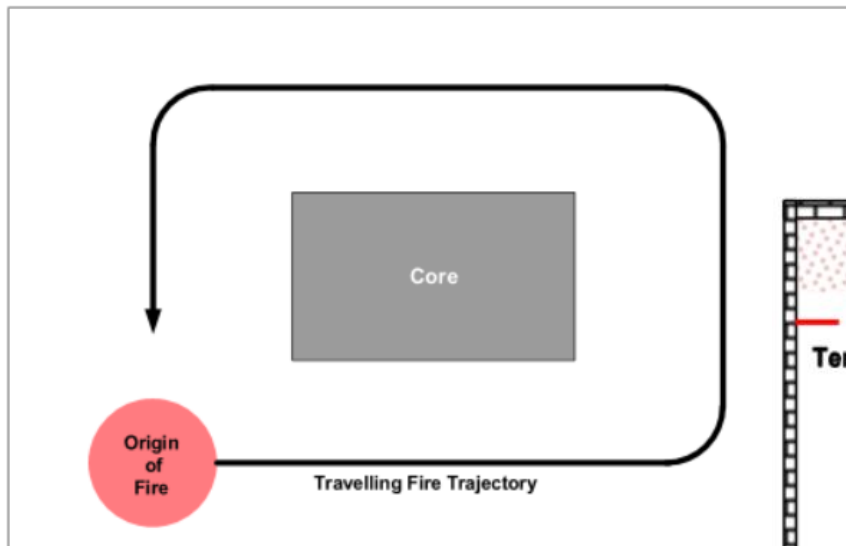
- Rackauskaite, Rein (2015)
 - Improvement of TFM – iTFM
 - Reducing range of fire sizes
 - Modifying T_{ff}
 - Flame flapping





Models of travelling fire

- Dai (2016)
 - Combination of Hasemi's localized fire and hot smoke layer
 - Propagation along a trajectory
 - Implementation into SIFBuilder

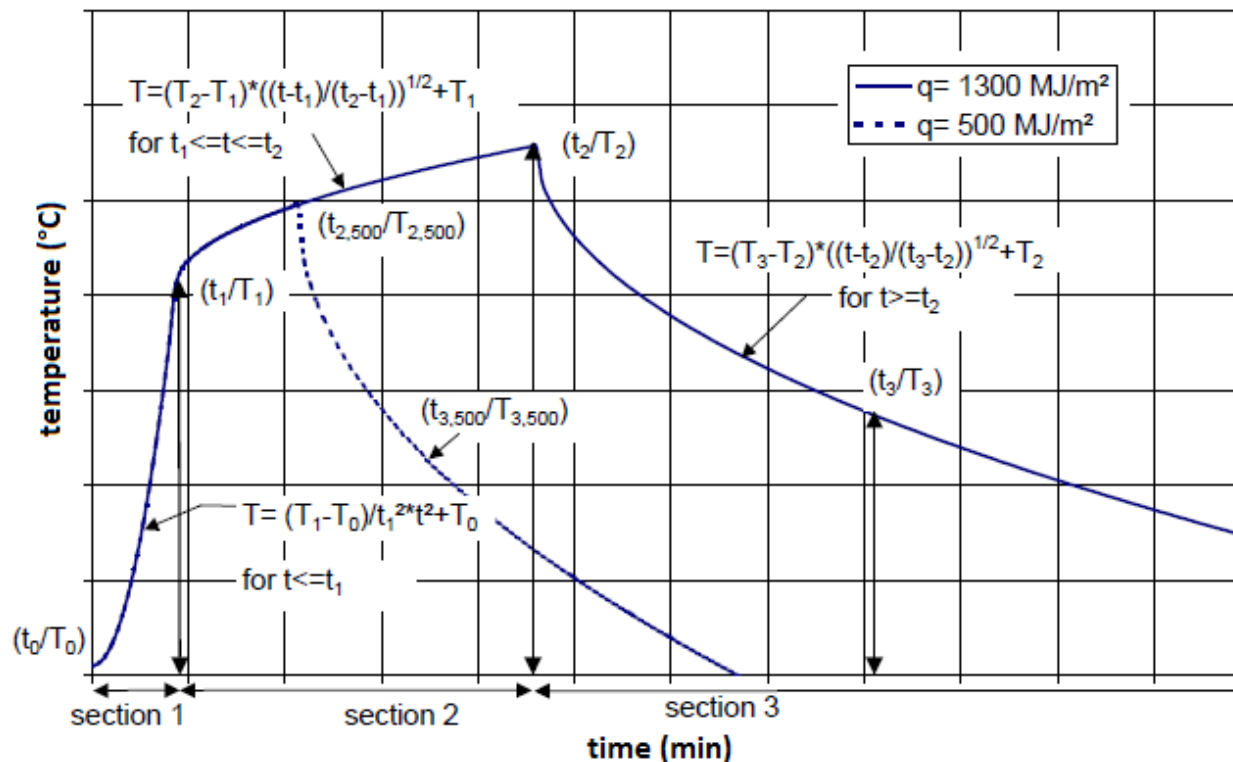




Models of travelling fire

HRR parametrical model

- Zehfuss, 2002
- Relationship with HRR – more realistic description of fire
- Implemented in DIN code

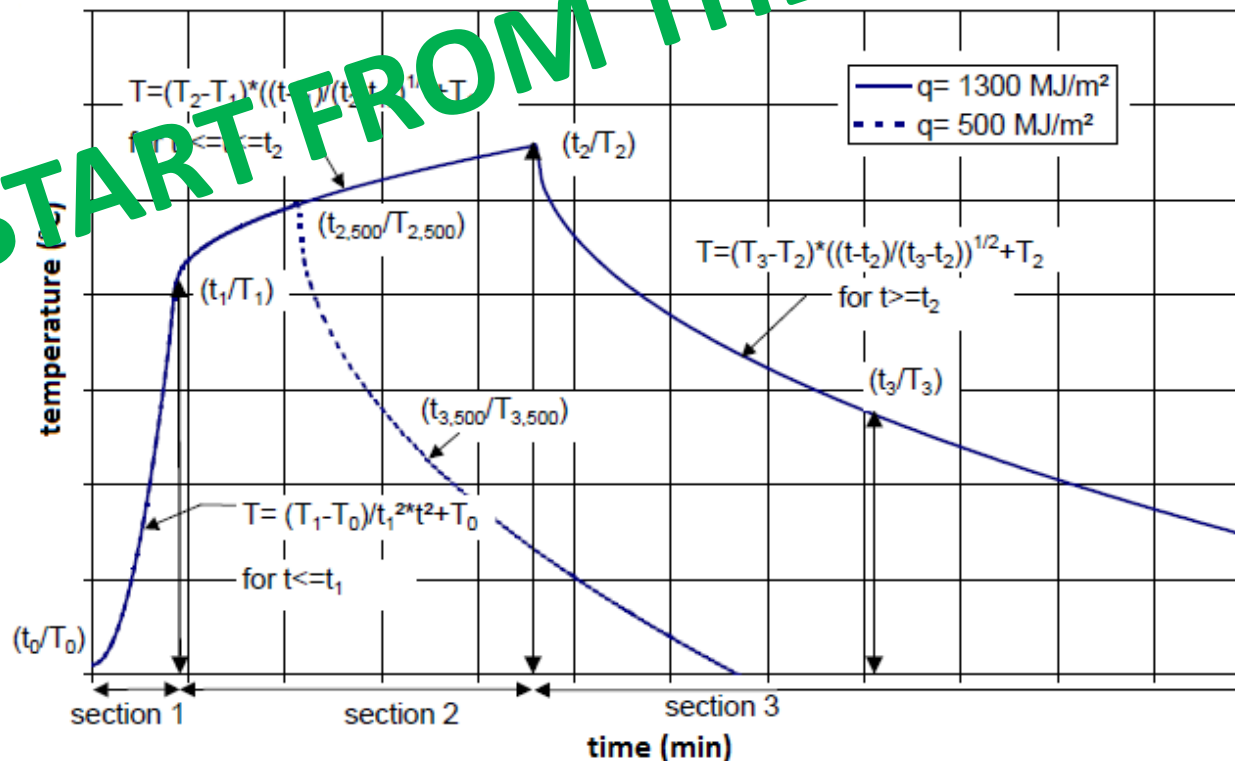




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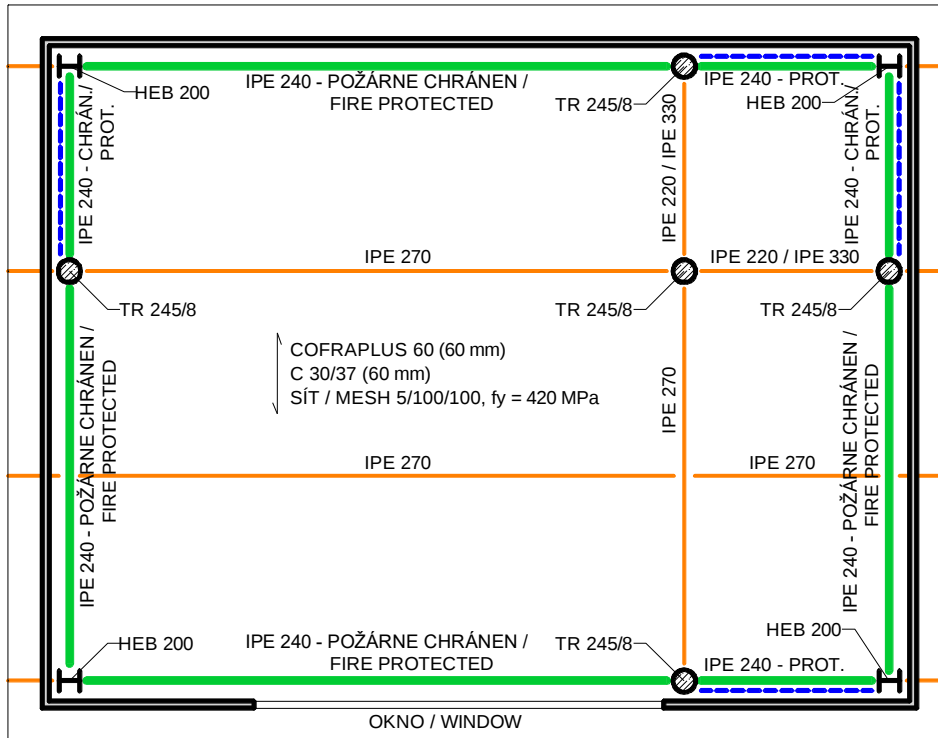




Experimental study

Fire Test in Veselí n. L.

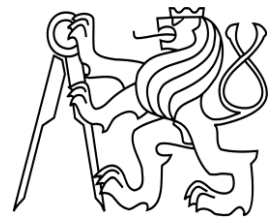
- 6th September 2011
- fire test on two floors administrative building
- travelling fire scenario in upper floor



- 10.4 x 13.4 x 9.0 m
- composite structure
- steel wires reinforcement
- IPE beams
- CFT columns
- window 2.0 x 5.0 m

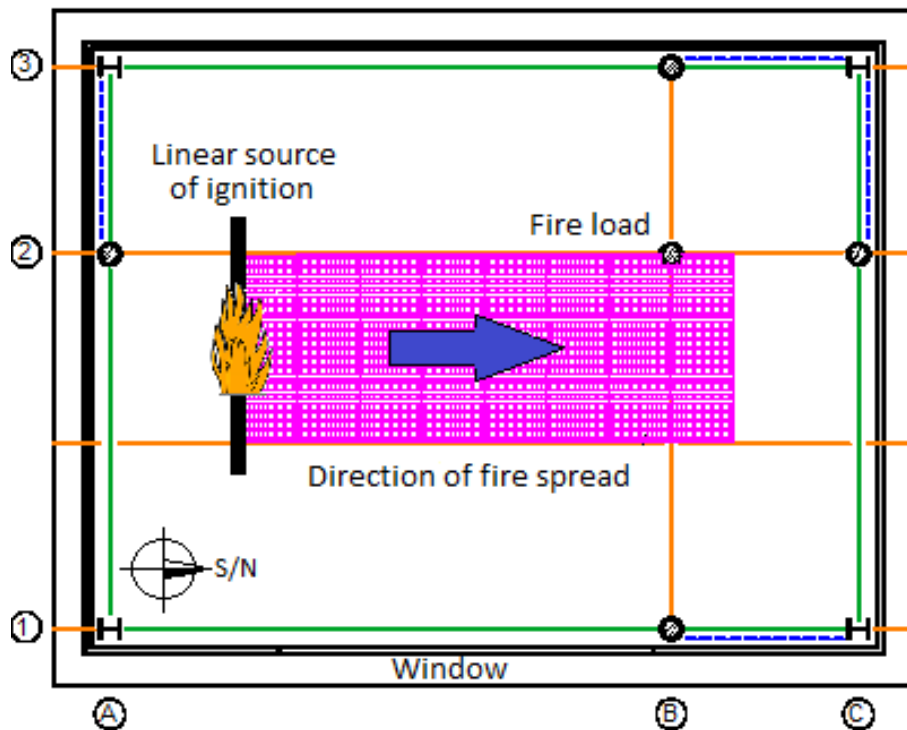
- 20 thermocouples $\varnothing$ 3 mm (gas)
- 8 thermocouples and 7 plate thermometers (steel beam)

Experimental study



Fire Test in Veselí n. L.

- 24 wooden piles on area of 24 m²
- 7 cribs of 50 x 50 x 1000 mm in 6 layers
- 2,52 m³ of wood (173,5 MJ/m²)
- linear ignition source
(U profile, mineral wool, paraffin)

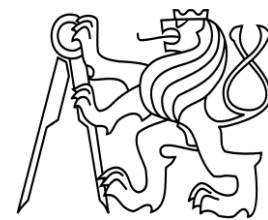


Fire load before the test



Fire load after the test

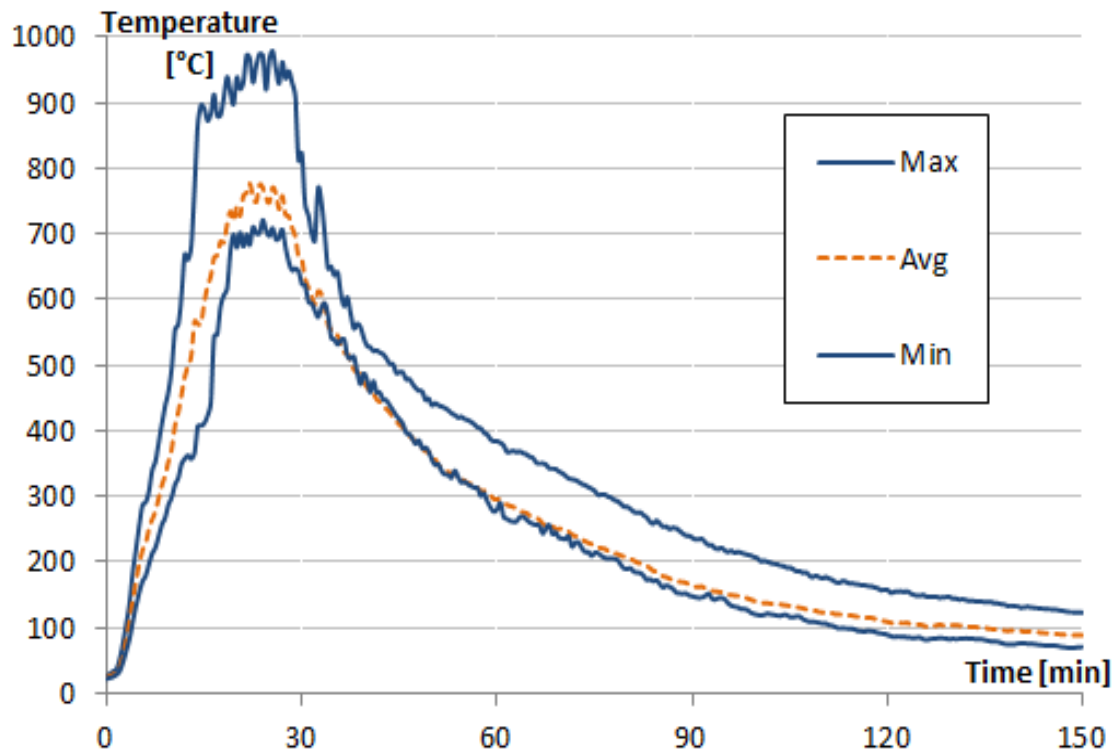
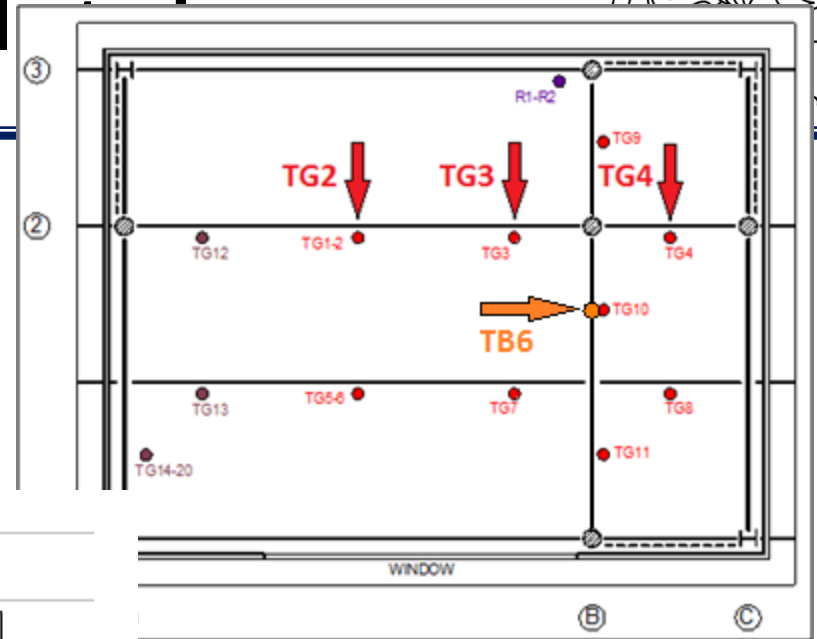
Experimental study





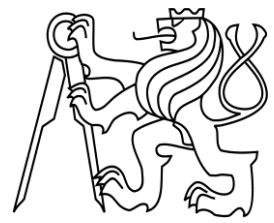
Experimental

- $T_{\max}$ 979 °C in 26. min, TG3
- **difference 400 °C, distance 6 m**
- $T_{\max}$ 855 °C at TB6

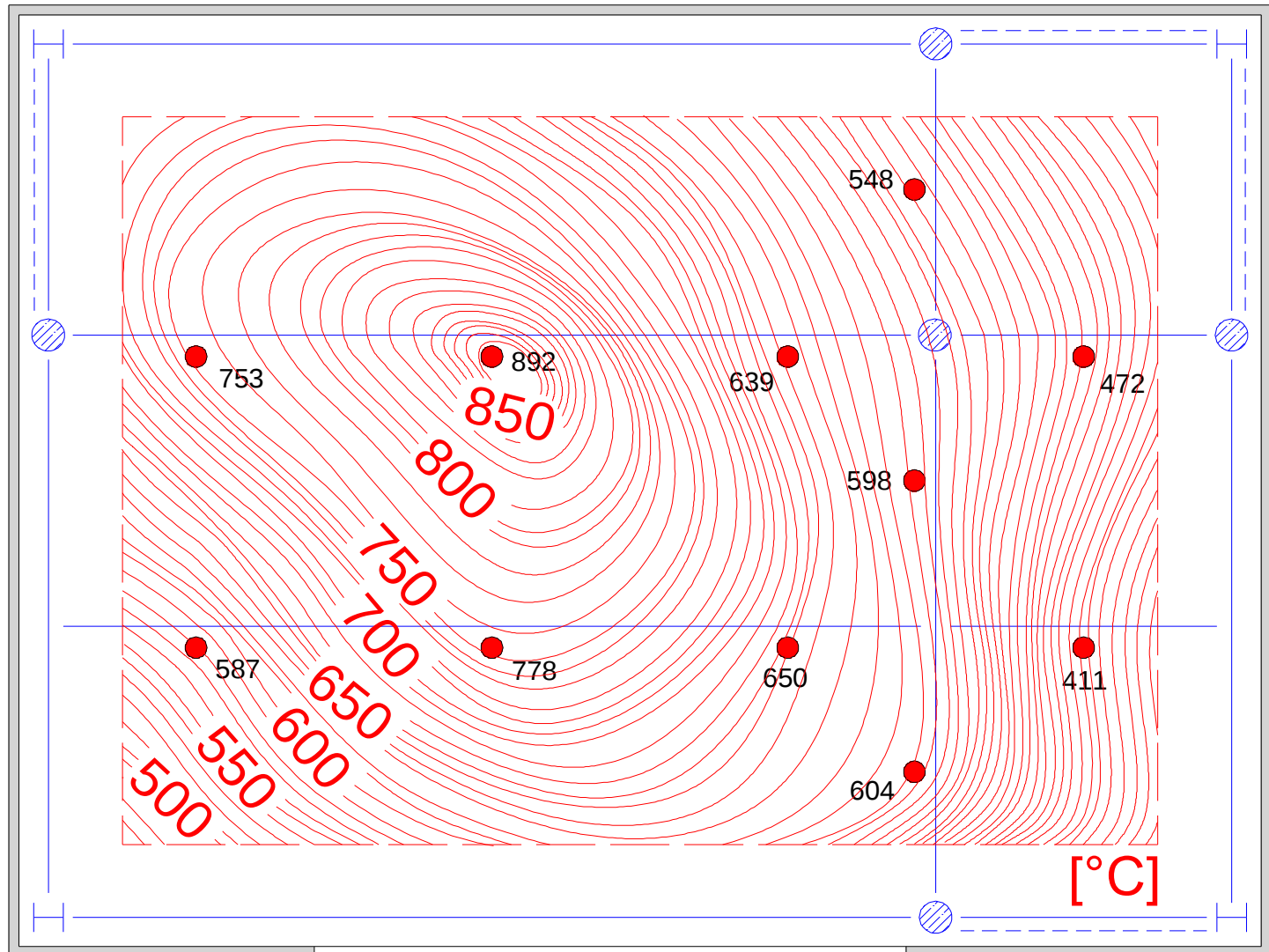


Time	TG2	TG3	TG4
[min]	[°C]	[°C]	[°C]
1.0	32.29	29.46	25.68
5.0	238.49	199.48	153.31
10.0	495.32	398.94	301.71
15.0	891.56	639.31	471.85
20.0	938.74	901.64	740.21
25.0	925.08	966.34	769.57
30.0	721.32	788.65	773.57

Experimental study



15 min

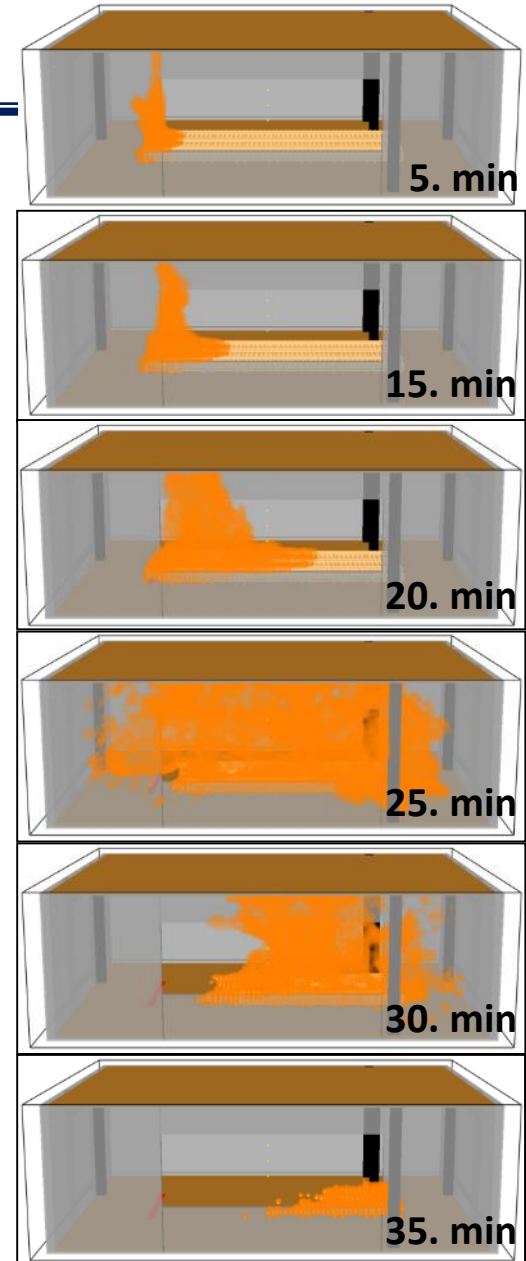


Numerical study

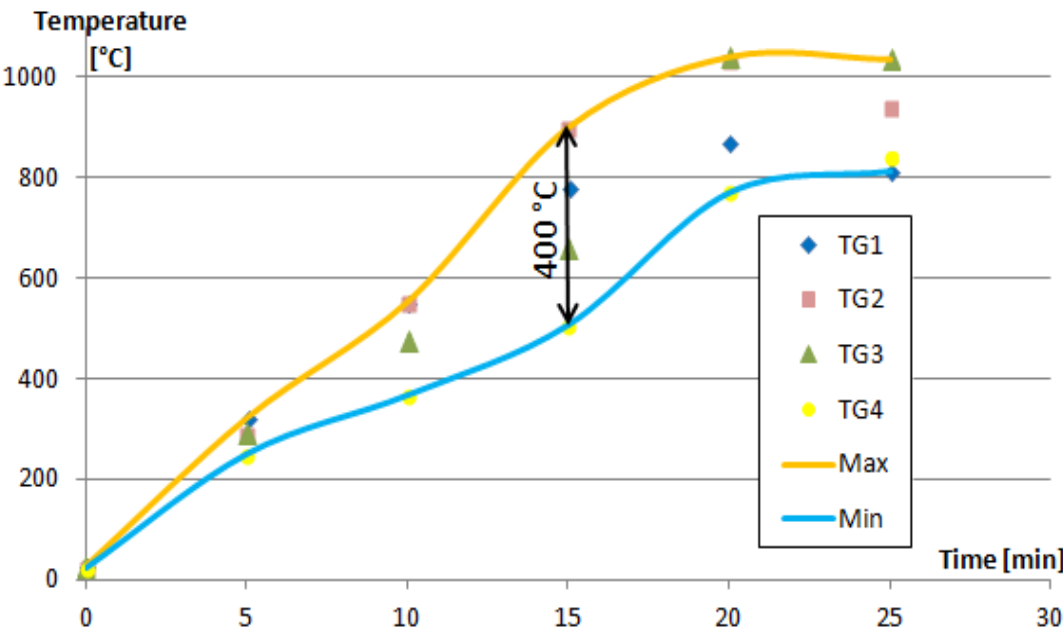
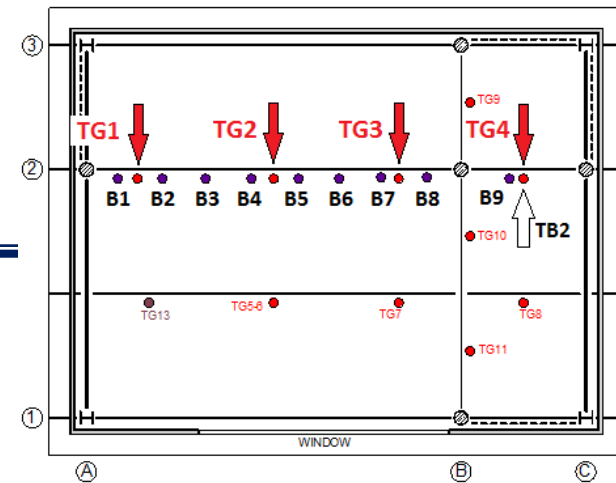


Software FDS (Fire Dynamics Simulator)

- model of FC from Veselí n. L.
- 4 materials → wood (cone calorimeter)
 T_{ign} , HRRPUA, ramp function
- fire outbreak „burner“ ($0.15 \times 3 \times 0.05 \text{ m}^3$)
→ HRRPUA, ramp func. (300 s)
- cell sizes: $10 \times 10 \times 10 \text{ cm}$, $5 \times 5 \times 5 \text{ cm}$
- calculation of RHR, gas temperature, beam temperature
- spreading phenomena and high degree of temperature heterogeneity confirmed

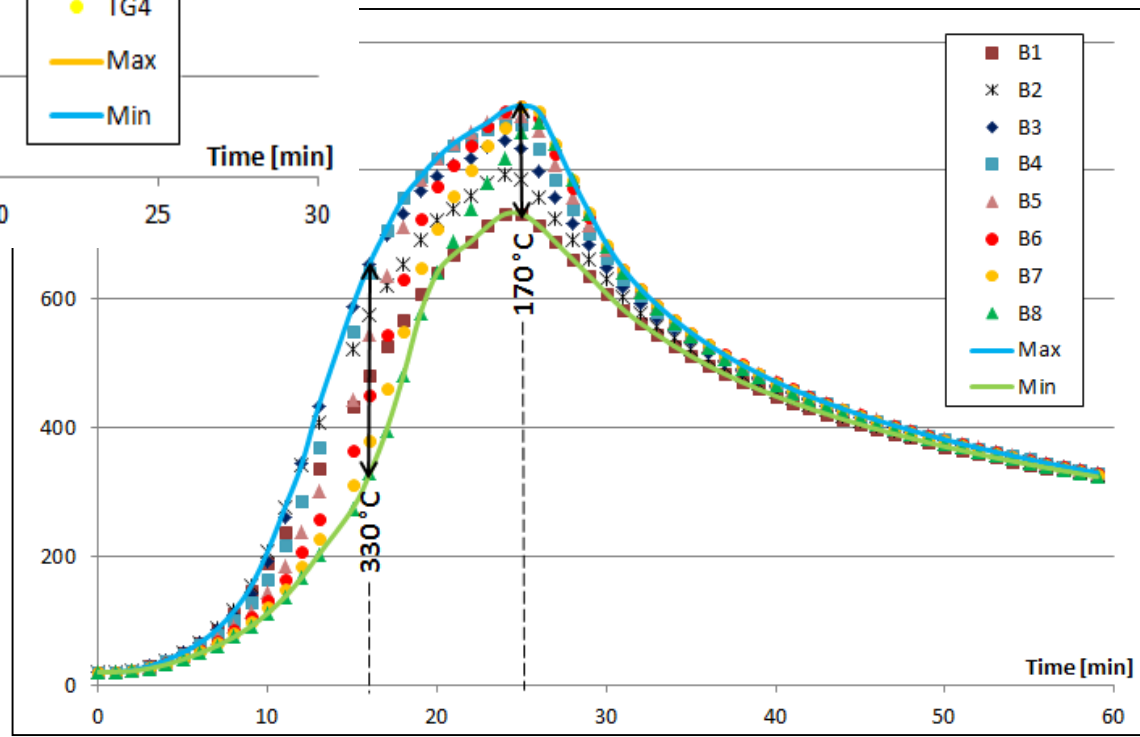


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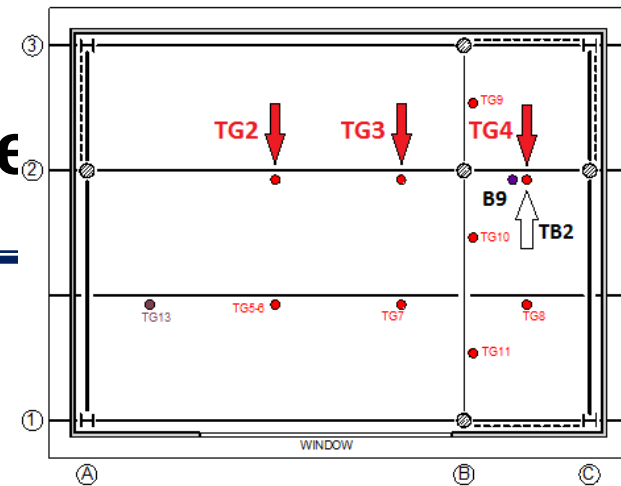
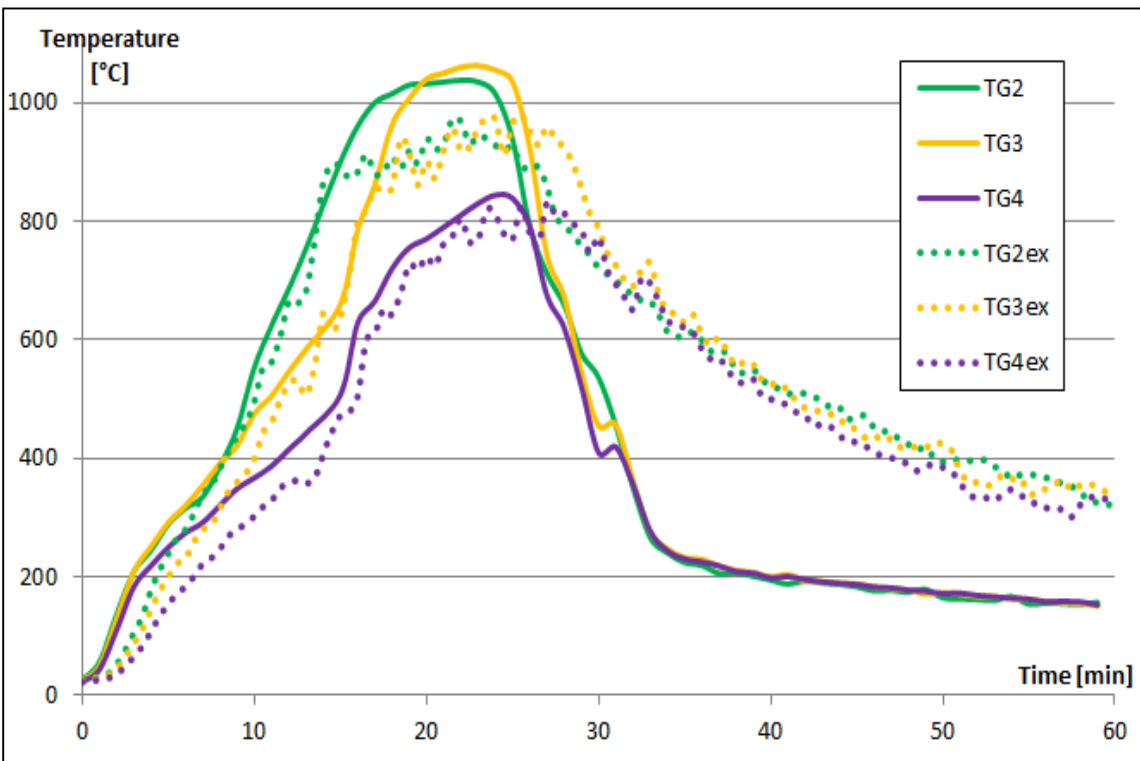


Gas temperature

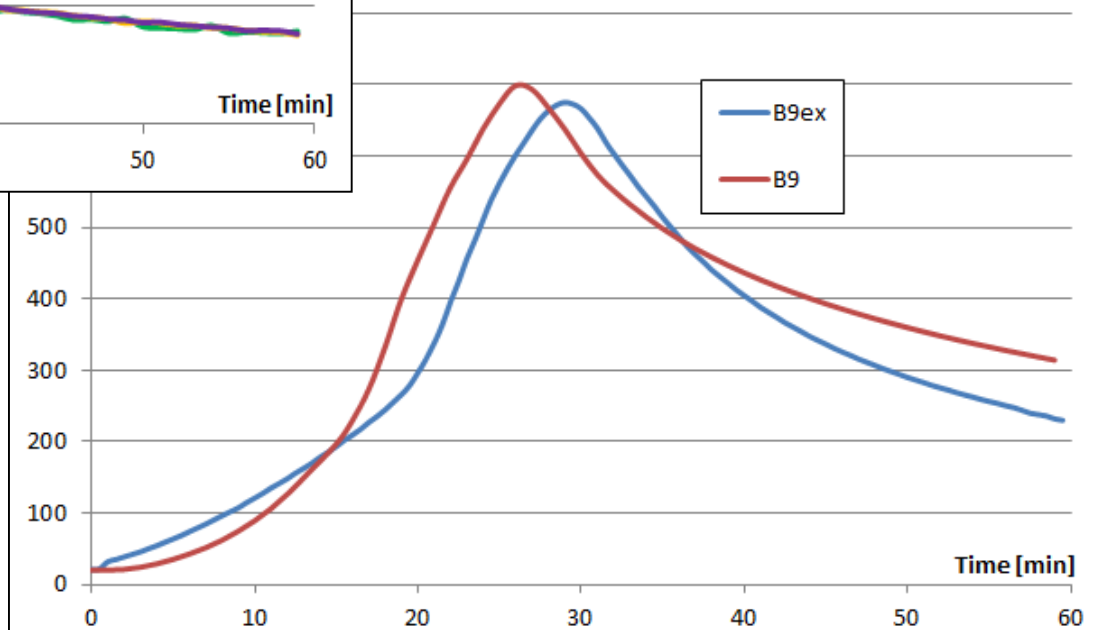
Steel beam temperature



Validation of the mode



Steel beam temperature



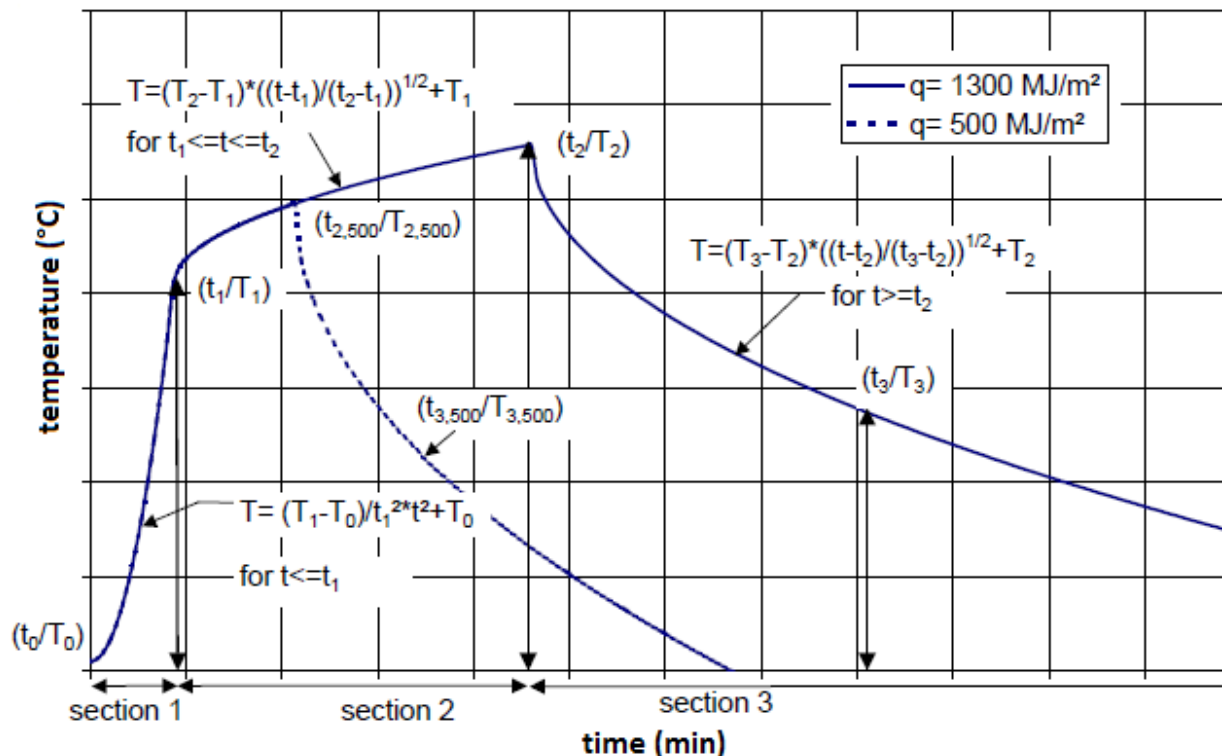
Gas temperature



Analytical model of TF

HRR parametrical model

- Zehfuss, 2002
- Relationship with HRR – more realistic description of fire
- Implemented in DIN code

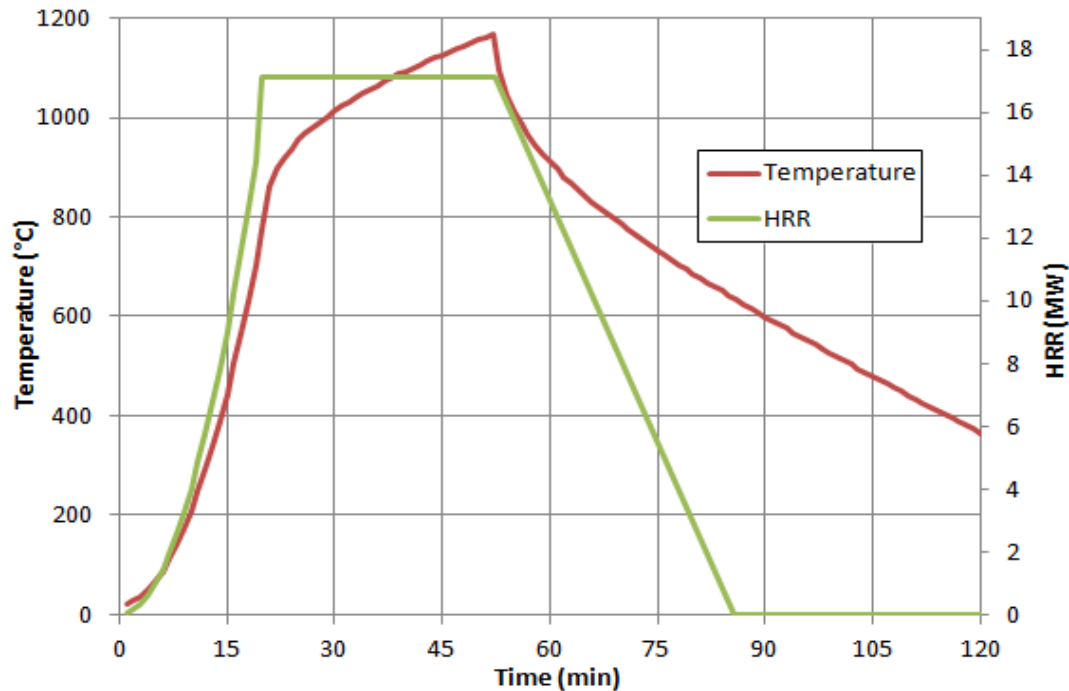




Analytical model of TF

Validation to fire test n. 2 in Veseli

- Uniformly distributed fire load (28 wooden piles)
- Fire load density 525 MJ/m²
- Ventilation opening 2 m x 5 m

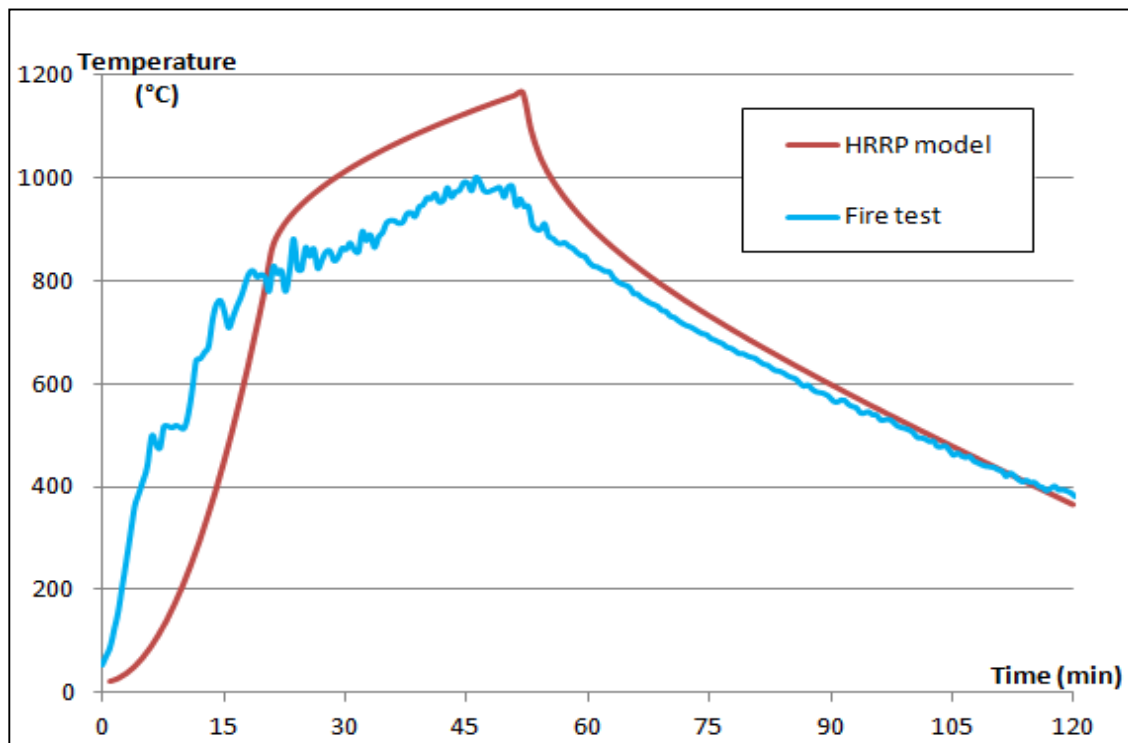


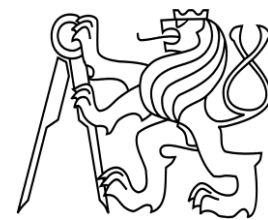


Analytical model of TF

Validation to fire test n. 2 in Veseli

- Lower temperature till 19 min
- Peak temperature 160°C higher
- Decay phase in good agreement

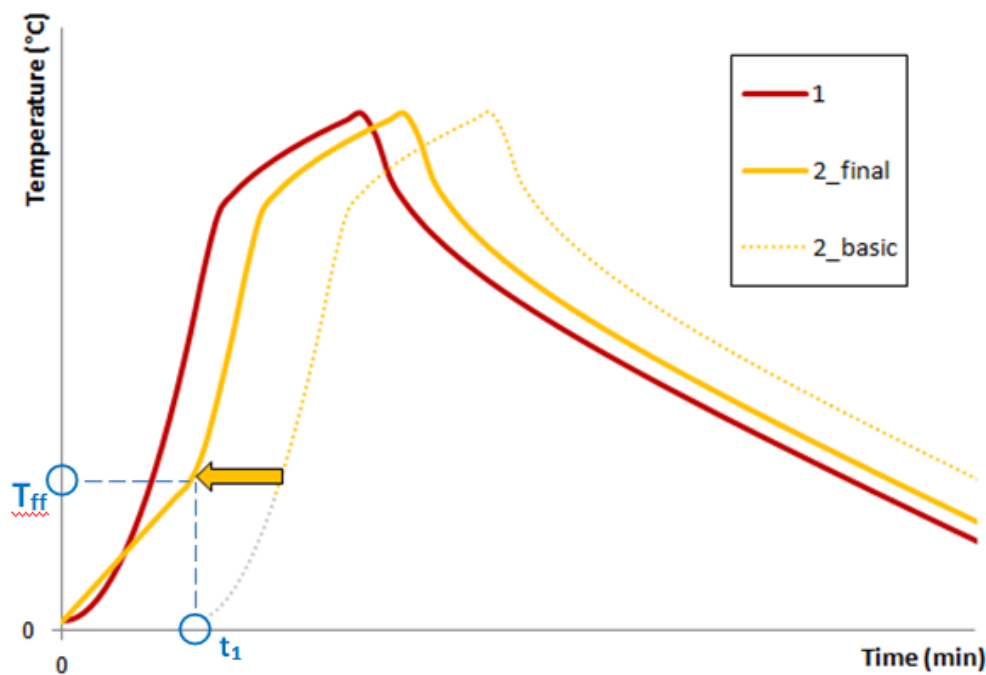




Analytical model of TF

Methodology

- Fire travels in one horizontal direction
- Division of enclosure into fields
- Temperature described by HRRP curve
- Spread rate influenced by HRR
 - $HRR_{max}(t_1)$ initiate curve 2
- Pre-heating given by T_{ff}
 - T_{ff} shifted back into t_1
 - Linear connection





Analytical model of TF

Methodology

- Fire travels in one horizontal direction
- Division of enclosure into fields
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- Spread rate influenced by HRR
 - $HRR_{\max}(t_1)$ initiate curve 2
- Pre-heating given by T_{ff}
 - T_{ff} shifted back into t_1
 - Linear connection

(Stern-Gottfried, 2011)

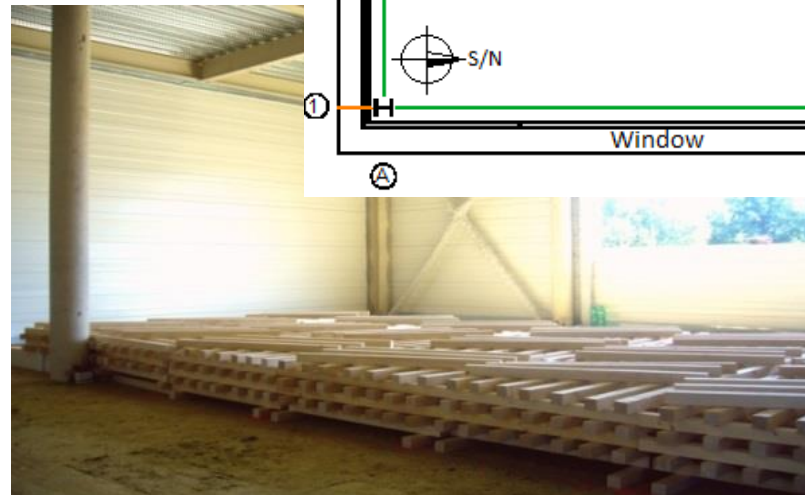
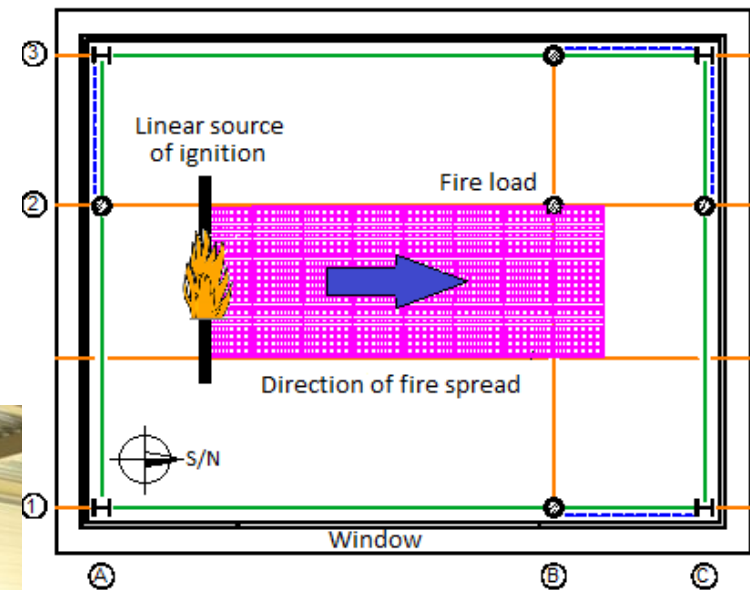
$$T_{ff} = \left[\frac{5}{3} \cdot \left(5.38 \frac{Q^{\frac{2}{3}}}{H} \right)^4 \cdot \frac{x_{nf}^{-\frac{5}{3}} - x_{ff}^{-\frac{5}{3}}}{x_{ff} - x_{nf}} + 4T_{\infty} \cdot \left(5.38 \frac{Q^{\frac{2}{3}}}{H} \right)^3 \cdot \frac{x_{nf}^{-1} - x_{ff}^{-1}}{x_{ff} - x_{nf}} + 18T_{\infty}^2 \cdot \left(5.38 \frac{Q^{\frac{2}{3}}}{H} \right)^2 \cdot \frac{x_{nf}^{-\frac{1}{3}} - x_{ff}^{-\frac{1}{3}}}{x_{ff} - x_{nf}} + 12T_{\infty}^3 \cdot \left(5.38 \frac{Q^{\frac{2}{3}}}{H} \right) \cdot \frac{x_{ff}^{\frac{1}{3}} - x_{nf}^{\frac{1}{3}}}{x_{ff} - x_{nf}} + T_{\infty}^4 \right]^{1/4}$$



Analytical model of TF

Validation to fire test n. 1 in Veseli

- Composite structure of 10.4 m x 13.4 m x 9.0 m
- Window 2.0 m x 5.0 m
- 24 wooden piles (2.52 m³ of wood)
- Linear ignition source
- No flashover – travelling fire

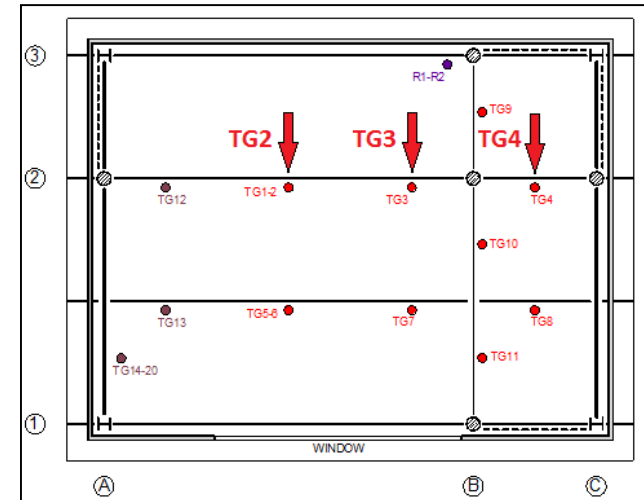




Analytical model of TF

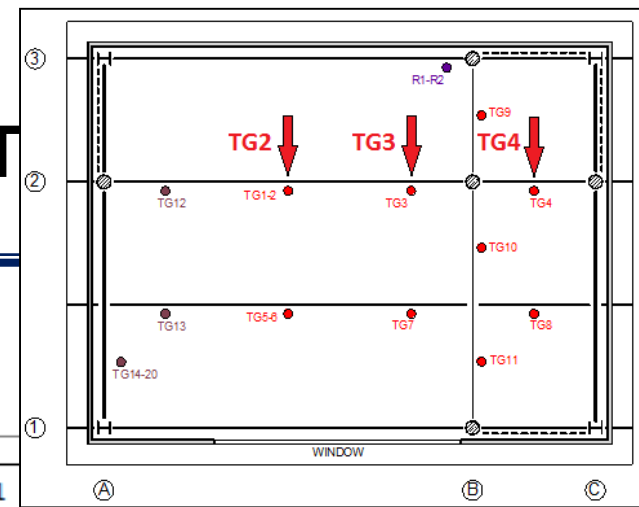
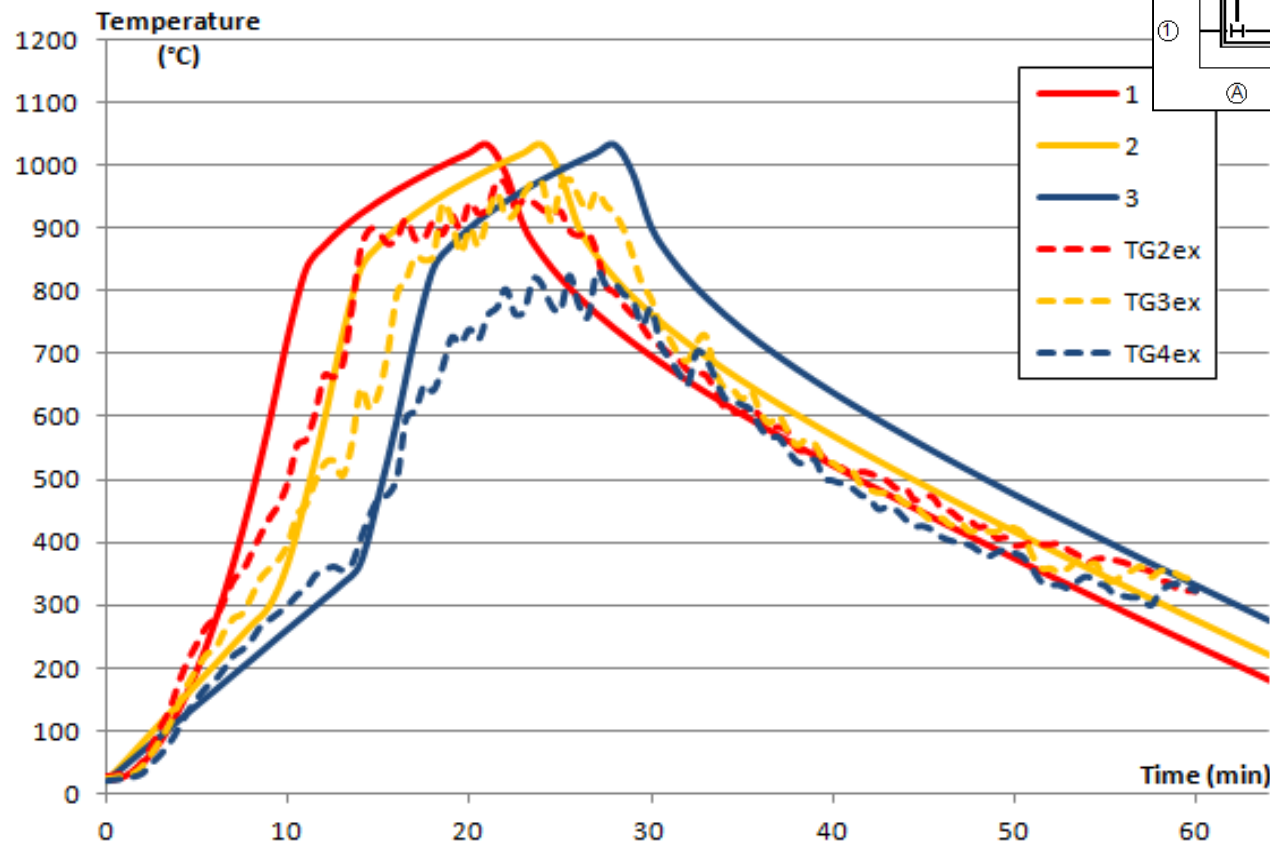
Validation to fire test n. 1 in Veseli

- Division into 3 fields
- Time t_α is equal to 150 s
- RHR_f is equal to 700 kW/m²
- Peak HRR = 16.8 MW
- Fuel-controlled fire
 - $t_1 = 10.25$ min
 - $t_2 = 21.83$ min
 - $t_3 = 34.49$ min
- Max temperature is 1020°C



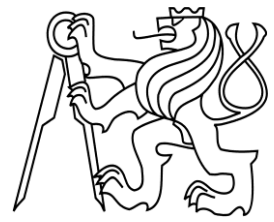
Analytical model of T

Validation to fire test n. 1 in Veseli



- Good agreement

Analytical model of TF - summary

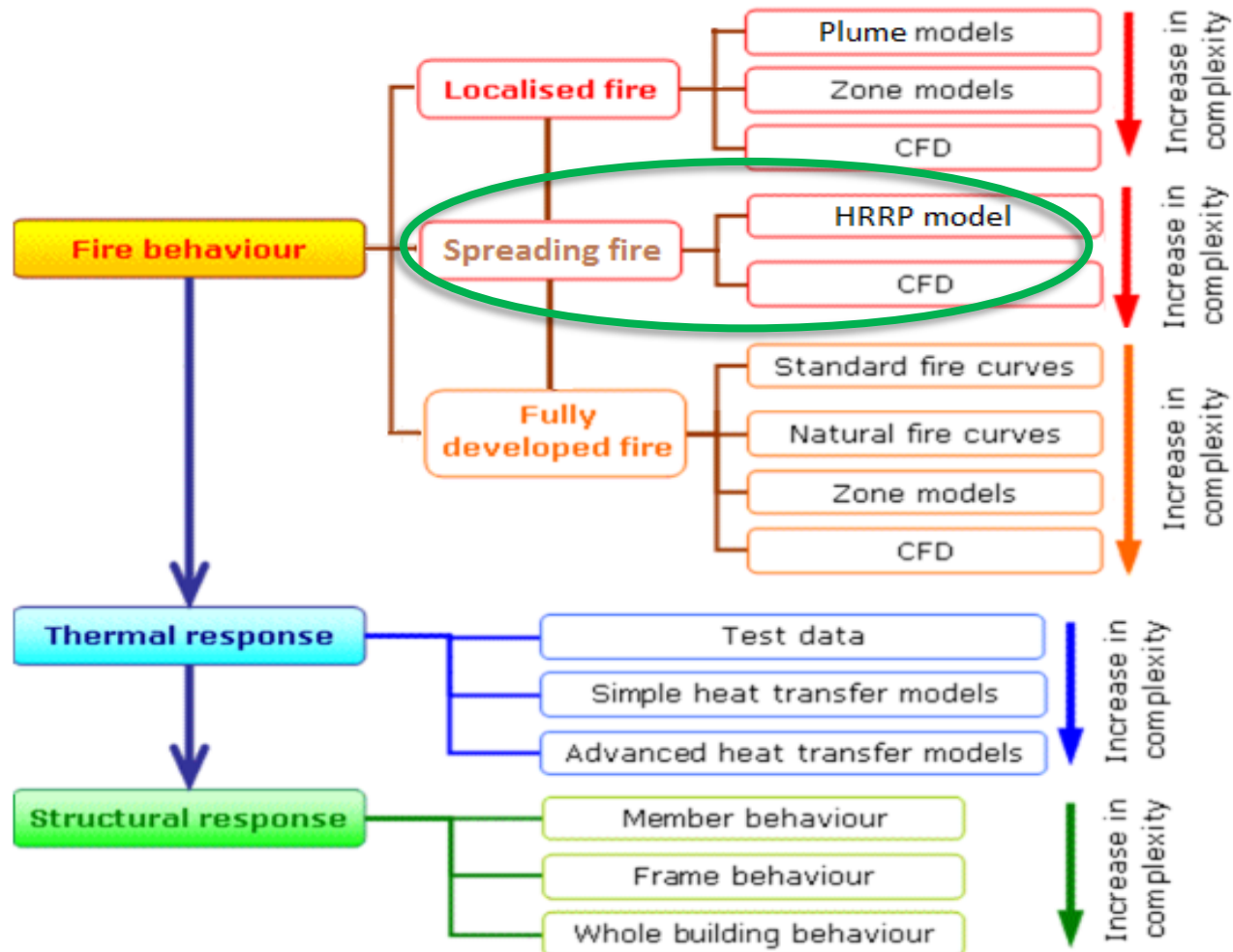


HRRP model of travelling fire

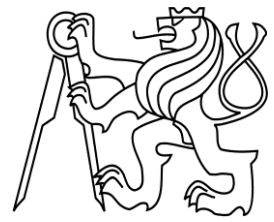
- Based on repetitious HRRP (iBMB) temperature-time curve
- Including pre-heating by application of T_{ff}
- Simple description of gas temperature during TF
- Investigate mechanical behaviour of structures involved in TF
- Validated to full-scale fire test in Veselí



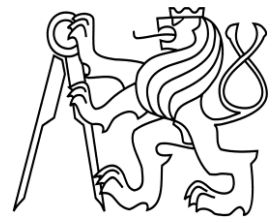
Analytical model of TF - summary



Summary



- The thermal analysis is often simplified to standard curve
- The standard curve is usually very conservative (compare to natural fire)
- Parametric curve can be used when more accurate solution is required. In this case, additional input data are required.
- Advanced mathematical models as zone model and CFD may be used for complex systems where simplified methods can not be applied.
- CFD is very complicated, it needs detailed input data, powerfull hardware, skilfull user, etc.
- Model of travelling fire may be implemented into the family of traditional design fire models.



Thank you for your attention!

kamila.cabova@fsv.cvut.cz



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